## APPENDIX B:

CONSTRUCTION HEALTH RISK ASSESSMENT
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# CenterStreet Garage Project for the City of Berkeley 

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## 1. Introduction

The City of Berkeley is proposing to redevelop an existing parking garage with a new parking garage on a 0.80 -acre parcel at 2025 Center Street in the City of Berkeley, Alameda County, California. The proposed Project would replace the existing five-story, 440 -space parking garage with an eight-level, 783 -space parking garage with micro-retail spaces, public accessible open space, secure bicycle parking and electric vehicle charging stations. Additionally, the Project would include garage operation space including offices, a break room, supply rooms, employee restrooms and storage.

The latest version of the BAAQMD CEQA Air Quality Guidelines requires projects to evaluate the impacts of construction activities on sensitive receptors (BAAQMD, 2012). Construction of the Project would take place starting in November 2015 and will include demolition, site preparation, grading, building construction, paving, and architectural coating (painting). The construction phase is estimated to take place over a period of 333 calendar days ( 238 work days) beginning in November 2015 and ending in November 2016.

The nearest off-site sensitive receptors (mixed-use multi-family residences) are located within 20 feet of the Project, adjacent to the Project site to the east along Center Street and adjacent to the site to the west along Addison Street. The residents at all of these locations could be potentially impacted from the proposed construction activities. Additionally, Berkeley City College is located approximately 70 feet south of the Project site, across Center Street, and Berkeley High School is located approximately 480 feet southwest of the Project site, at 1980 Allston Way. The students and adult staff at these school locations could also be potentially impacted from the proposed construction activities. Therefore, a site-specific construction health risk assessment (HRA) was prepared for the Project.

This construction HRA considers the health impact of construction operations at the Project site to sensitive receptors (adults and children in the nearby residences and students and staff of Berkeley City College and Berkeley High School) from diesel equipment exhaust and particulate matter $\left(\mathrm{PM}_{2.5}\right)$.

## 1. Introduction

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## 2. Project Description

The Project site is located on a 0.80 acre site at 2025 Center Street in the City of Berkeley, Alameda County, California. The proposed Project would replace the existing five-story, 440 -space parking garage with an eight-level, 783 -space parking garage with micro-retail spaces, public accessible open space, secure bicycle parking and electric vehicle charging stations. Additionally, the Project would include garage operation space including offices, a break room, supply rooms, employee restrooms and storage. Construction of the Project is anticipated to begin in November 2015 and be completed in November 2016.

The existing garage is located in Downtown Berkeley within close proximity to a variety of land uses. On the Addison Street frontage, the Project site is adjoined by commercial uses to the east, and mixed-use commercial and residential uses to the west. On the Center Street frontage, the Project site is adjoined by restaurants as well as residential, institutional, and commercial uses. Berkeley City College is located across Center Street from the existing garage. Berkeley High School is located approximately 480 feet southwest of the Project site, at 1980 Allston Way.

The project site and vicinity are depicted in Figure 1.
2. Project Description

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Date: February 2015
Figure 1
Project Location and ISCST3 Model Configuration
2. Project Description

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## 3. Methodology and Significance Thresholds

The purpose of the construction HRA is to evaluate the potential health impacts from diesel particulate matter (DPM) and particulate matter less than 2.5 microns $\left(\mathrm{PM}_{2.5}\right)$ emitted during construction activities associated with the proposed project. Construction sources evaluated in this HRA include off-road construction equipment, such as excavators, graders, forklifts, pavers, rollers, dozers, tractors/loaders/backhoes, concrete saws, crushing/processing equipment, air compressors, generators, cement and mortar mixers, cranes, caisson drill rig, and water trucks.

The BAAQMD's 2010 adopted "Thresholds of Significance" for local community risk impacts were challenged in a lawsuit and subsequently rescinded. However, lead agencies can determine that these are appropriate air quality thresholds for projects they review. The 2010 BAAQMD thresholds that were used for this project are shown below:

- Non-compliance with a qualified risk reduction plan
- Excess cancer risk of more than 10 in a million
- Non-cancer hazard index (chronic or acute) greater than 1.0
- Incremental increase in average annual $\mathrm{PM}_{2.5}$ concentration of greater than $0.3 \mu \mathrm{~g} / \mathrm{m}^{3}$

Since both the City of Berkeley and Alameda County do not currently have qualified risk reduction plans, a site-specific analysis of DPM and $\mathrm{PM}_{2.5}$ impacts on sensitive receptors was conducted. The methodology used in this HRA is consistent with the following BAAQMD and the Office of Environmental Health Hazard Assessment (OEHHA) guidance documents:

- BAAQMD, 2012. California Environmental Quality Act Air Quality Guidelines. May 2012.
- BAAQMD, 2011. Recommended Methods for Screening and Modeling Local Risks and Hazards. Version 2.0. May 2011
- OEHHA, 2012. Air Toxics Hot Spots Program Risk Assessment Guidelines. Revised Technical Support Document for Exposure Assessment and Stochastic Analysis. August, 2012.
- OEHHA, 2003. The Air Toxics Hot Spots Program Guidance Manual for Preparation of Health Risk Assessments. August, 2003.

Potential exposures to DPM and $\mathrm{PM}_{2.5}$ from proposed project construction activities were evaluated for offsite sensitive receptors in close proximity to the Site, including the residences to the west and east, and staff and students at Berkeley City College to the south and at Berkeley High School to the southwest. Using air dispersion models, receptor concentrations were estimated and excess lifetime cancer risks and chronic noncancer hazard indexes were calculated. These risks were then compared to the significance thresholds identified in the BAAQMD CEQA guidelines.

## 3. Source Identification

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## 4. Construction Emissions

Construction emissions were calculated as average daily emissions in pounds per day, using the proposed construction schedule and the latest version of California Emissions Estimation Model, known as CalEEMod Version 2013.2.2 (CAPCOA, 2013).

The project was assumed to take place over 377 calendar days ( 270 work days) beginning in November 2015 and ending in November 2016. The average daily emission rates from construction equipment used during the proposed Project were determined by dividing the annual average emissions for each construction year by the number of construction days per year. In addition, emissions from haul trucks traveling to and from the site within a 1,000 -foot radius were included as off-site emissions. The modeled average daily emission rates for the construction scenario are summarized in Table 1. The CalEEMod construction emissions output and emission rate calculations are provided in Appendix A.

Table 1 Construction Activity

| Parameter - Year | On-site Emissions (lbs/day) | Total Off-site Emissions (lbs/day) |
| :---: | :---: | :---: |
| DPM - 2015 | 1.97 | 0.16 |
| DPM - 2016 | 2.90 | 0.06 |
| $\mathrm{PM}_{2.5}-2015$ | 2.29 | 0.36 |
| $\mathrm{PM}_{2.5}-2016$ | 2.83 | 0.34 |

Presented emission rates are average daily emissions, with BAAQMD's Best Management Practices (BMPs) for Fugitive Dust.
Source: CalEEMod 2013.2.2.

## 4. Source Characterization

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## 5. Dispersion Modeling

To assess the impact of emitted compounds on sensitive receptors near the Project, air quality modeling using the ISCST3 atmospheric dispersion model was performed. The model is a steady state Gaussian plume model and is an approved model by BAAQMD for estimating ground-level or flagpole-level impacts from point and fugitive sources in simple and complex terrain. The on-site construction emissions for the project were modeled as poly-area sources. Off-site construction emissions for project related truck traffic were modeled as adjacent volume sources.

The model requires additional input parameters, including chemical emission data and local meteorology. Inputs for the construction phase emission rates are those described in Section 4. Meteorological data obtained from the BAAQMD for the nearest met station (UC Richmond) and the three latest available years of record (2003-2005) were used to represent local weather conditions and prevailing winds.

DPM emissions were based on the CalEEMod construction runs, using annual exhaust $\mathrm{PM}_{10}$ construction emissions presented in $\mathrm{lbs} /$ day. The $\mathrm{PM}_{2.5}$ emissions were taken from the CalEEMod $\mathrm{PM}_{2.5}$ total, which includes exhaust $\mathrm{PM}_{2.5}$ as well as fugitive dust $\mathrm{PM}_{2.5}$. Off-site construction emissions from haul trucks were also obtained from the CalEEMod construction runs, proportioning the emissions for the haul truck trips of 20 miles to take into account the 0.26 mile route within 1,000 feet of the project site. An emission release height of 4.15 meters was used as representative of the stack exhaust height for off-road construction equipment and off-site haul trucks and an initial vertical dispersion parameter of 1.93 m was used, per CARB guidance (2000). The lateral dispersion parameter for the truck volume sources along Milvia Street and University Avenue was determined by dividing the width of the traveled roadway by 2.15 .

The modeling analysis also considered the spatial distribution and elevation of each emitting source in relation to the sensitive receptors. To accommodate the model's Cartesian grid format, direction-dependent calculations were obtained by identifying the Universal Transverse Mercator (UTM) coordinates for each source location.

To determine contaminant impacts during construction hours, the model's scalar option was invoked to predict flagpole-level concentrations ( 1.5 m for ground-floor receptors, 6.1 m for second-floor receptors, and 9.14 m for third-floor receptors) for emissions generated between the hours of 7:00 AM and 4:00 PM, with a one-hour break for lunch between noon and 1:00 PM. In addition, a scalar factor was applied to the risk calculations to account for the number of days of construction activity per year.

For all modeling runs, a unit emission rate of $1 \mathrm{gm} / \mathrm{sec}$ was used. The unit emission rates were proportioned among either the volume sources for truck traffic, or proportioned over the poly-area sources for on-site construction emissions. The maximum ISCST3 concentrations from the output files were then multiplied by the emission rates calculated in Appendix A to obtain the maximum flagpole-level concentrations at the maximum exposed receptor (MER) near the Project site for each receptor type. Separate MER locations were

## 5. Exposure Quantification

determined for residential receptors, Berkeley City College, and Berkeley High School. The flagpole-level DPM and $\mathrm{PM}_{2.5}$ concentrations from the on-site and off-site sources used in the risk calculation spreadsheets are provided in Table C1 of Appendix C. The ISCST3 model output for the emission sources is presented in Appendix B. The configuration of the sources and the receptor locations is presented in Figure 1.

## 6. Risk Characterizations

### 6.1 CARCINOGENIC CHEMICAL RISK

The BAAQMD has established a threshold of ten in a million (10E-06) as a level posing no significant risk for exposures to carcinogens.

Health risks associated with exposure to carcinogenic compounds can be defined in terms of the probability of developing cancer as a result of exposure to a chemical at a given concentration. The cancer risk probability is determined by multiplying the chemical's annual concentration by its cancer potency factor (CPF), a measure of the carcinogenic potential of a chemical when a dose is received through the inhalation pathway. It is an upper-limit estimate of the probability of contracting cancer as a result of continuous exposure to an ambient concentration of one microgram per cubic meter $\left(\mu \mathrm{g} / \mathrm{m}^{3}\right)$ over a lifetime of 70 years.

Cancer risks were calculated using BAAQMD recommended methods for a residential receptor. For the inhalation pathway, contaminant dose is multiplied by the cancer potency factor in units of inverse dose expressed in milligrams per kilogram per day $(\mathrm{mg} / \mathrm{kg} / \text { day })^{-1}$ to derive the cancer risk estimate. To calculate the contaminant dose, the following equation was used:

$$
\text { Do se }_{A R R}=\left(C_{a i r} \times E F \times E D \times[B R / B W] \times A \times C F\right) / A T
$$

Where:

| Do se ${ }_{\text {ald }}$ | = | dose by inhalation (mg/kg/day) |
| :---: | :---: | :---: |
| $\mathrm{Cair}_{\text {ar }}$ | = | concentration of contaminantin air ( $\mu \mathrm{g} / \mathrm{m}^{3}$ ) |
| EF | = | exposure frequency (days/year) |
| ED | = | exposure duration (years-construction peniod) |
| BR/BW | = | daily breathing rate no malize d to body we ight (L/kg-day) |
| A | = | inhalation absorption factor (de fault = 1) |
| CF | = | conversion factor ( $1 \times 10^{-6}, \mu \mathrm{~g}$ to mg , Lto $\mathrm{m}^{3}$ ) |
| AT | = | averaging time (days) |

The inhalation absorption factor (A) is a unitless factor that is only used if the cancer potency factor included a correction for absorption across the lung. For this assessment, the default value of 1 was used. The daily breathing rate for an adult is $302 \mathrm{~L} / \mathrm{kg}$-day and for a child is $581 \mathrm{~L} / \mathrm{kg}$-day (BAAQMD, 2012). The residential exposure frequency (EF) is set at 350 days per year to allow for a two week period away from home each year (OEHHA, 2012). To represent the unique characteristics of school populations (e.g. Berkeley City College and Berkeley High School), the assessment employed the USEPA's guidance to develop viable dose estimates based on reasonable maximum exposure, defined as the "highest exposure that is reasonably expected to occur" for a given receptor population. Lifetime risk values for the student population were adjusted to account for an exposure of 180 days per year for 9 years. OEHHA does not support the use of current cancer potency factor to evaluate cancer risk for exposures of less than 9 years (OEHHA, 2003). To assess staff-related risk, exposures were adjusted to account for an employment period of 240 days per year

## 6. Risk Characterizations

(OEHHA, 2012). The daily breathing rate for adult staff and adult students is $302 \mathrm{~L} / \mathrm{kg}$-day, and for high school students is $451 \mathrm{~L} / \mathrm{kg}$-day (OEHHA, 2003). The AT (averaging time) for lifetime cancer risks is 70 years for all cases.

OEHHA and BAAQMD procedures require the incorporation of age sensitivity factors (ASF) into the evaluation. The exposure duration (ED) and ASFs for the various age-groups are provided herein:

| $\frac{\mathrm{ED}}{0.25}$ years - third trimester | 10 |
| :--- | :--- |
| 2 years for 0-2 age group | 10 |
| 7 years for 2-9 age group | 3 |
| 14 years for 2-16 age group | 3 |
| 54 years for 16-70 age group | 1 |

To calculate the overall cancer risk, the risk for each appropriate age group is calculated using appropriate age-sensitivity factors (ASFs), chemical-specific cancer potency factor (CPF) for each chemical of concern, and the fraction of time at home (FAH) as per the following equation:

$$
\text { Cance erisk }{ }_{A R R}=\text { Do se }_{\text {AIR }} x \text { CPF } x \text { ASF } x \text { FAH }
$$

The CPFs used in the assessment were obtained from OEHHA guidance. For DPM, a CPF of $1.1 \mathrm{mg} / \mathrm{kg}-$ day ${ }^{-1}$ was used.

The excess lifetime cancer risk to the maximally exposed receptor (MER) during the construction period was calculated, based on the factors provided above. For the adult resident exposure scenario, an ASF of 1.7 was applied to the calculated cancer risk number to give the estimated excess cancer risk over a 70 -year lifetime. For the child resident exposure scenario, a 9-year exposure period was used, as per BAAQMD and OEHHA guidance (BAAQMD, 2012). In addition, an ASF of 4.7 was applied to the excess cancer risk number to account for the increased sensitivity of children to air pollutants during the 9-year exposure period. Finally, a fraction of time at home (FAH) was applied, as per OEHHA guidance (OEHHA, 2012). For the unmitigated scenario, a FAH factor of 1 was assumed. The calculated risk for high school students is multiplied by an ASF weighting factor of 3 (for children ages 2 to 16) to account for early life sensitivity to pollutant exposures (OEHHA, 2012). For adult staff and adult students, an ASF of 1.0 was applied to the excess cancer risk.

The calculated results are provided in Appendix C.

## 6. Risk Characterizations

### 6.2 NON-CARCINOGENIC HAZARDS

An evaluation of the potential non-cancer effects of chronic chemical exposures was also conducted. Adverse health effects are evaluated by comparing the annual receptor level (flagpole) concentration of each chemical compound with the appropriate reference exposure limit (REL). Available RELs promulgated by OEHHA were considered in the assessment.

To quantify non-carcinogenic impacts, the hazard index approach was used. The hazard index assumes that chronic sub-threshold exposures adversely affect a specific organ or organ system (toxicological endpoint). For each discrete chemical exposure, target organs presented in regulatory guidance were used. To calculate the hazard index, each chemical concentration or dose is divided by the appropriate toxicity value. For compounds affecting the same toxicological endpoint, this ratio is summed. Where the total equals or exceeds one, a health hazard is presumed to exist. In a manner consistent with the assessment of carcinogenic exposures, REL/RfC (reference concentration) values were converted to units expressed in $\mathrm{mg} / \mathrm{kg} /$ day to accommodate the above intake algorithm.

The chronic hazard analysis for DPM is provided in Appendix C. The calculations contain the relevant exposure concentrations and corresponding reference dose values used in the evaluation of non-carcinogenic exposures.

### 6.3 CRITERIA POLLUTANTS

The BAAQMD has recently incorporated $\mathrm{PM}_{2.5}$ into the District's CEQA significance thresholds due to recent studies that show adverse health impacts from exposure to this pollutant. An incremental increase of greater than $0.3 \mu \mathrm{~g} / \mathrm{m}^{3}$ for the annual average $\mathrm{PM}_{2.5}$ concentration is considered to be a significant impact. The modeling results for $\mathrm{PM}_{2.5}$ are summarized in Table 2 and Table 4; the model runs are provided in Appendix B.

## 6. Risk Characterizations

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## 7. Conclusions

The residential health risk values are based on the maximum modeled receptor concentration over the construction exposure period, conservatively assuming a 24 -hour outdoor exposure and averaged over a 70year lifetime. According to the modeling results, the overall MER is an off-site multi-family residence immediately east of the Project. Results of the HRA indicate that the maximum adult incremental cancer risk during the construction phase of the Project at the residential MER is 8.6 per million, which is less than the significance threshold of 10 per million. However, the incremental cancer risk for the child exposure scenario was estimated to be 45 per million, which exceeds than the significance threshold of 10 per million. Therefore, mitigation measures are warranted. For adult students and staff at Berkeley City College, and adult staff and students at Berkeley High School, the incremental cancer risk did not exceed BAAQMD's significance threshold.

For non-carcinogenic effects, the hazard index identified for each toxicological endpoint totaled less than one for all receptors. Therefore, chronic non-carcinogenic hazards are within acceptable limits. Lastly, the $\mathrm{PM}_{2.5}$ annual concentrations generated by construction emissions during 2016 are greater than the BAAQMD significance threshold at the residential MER location and at Berkeley City College. The unmitigated health risk results for all receptors are summarized in Table 2.

Table 2 Health Risk Assessment Results

| Receptor | Cancer Risk <br> (per million) | Chronic Hazard Index |
| :--- | :---: | :---: | :---: | | $\mathbf{P M}_{2} .5$ <br> $\left(\boldsymbol{\mu g} / \mathrm{m}^{3}\right)$ |
| :---: |
| Adult Resident |
| Child Resident |
| Berkeley City College Adult Student/Staff |
| Berkeley High School Student |
| Berkeley High School Staff |
| BAAQMD Threshold |
| Exceeds Threshold |
| Sources: (Lakes AERMOD View, 8.8.1, 2014). |

It should be noted that these health impacts were based on conservative (i.e., health protective) assumptions. The USEPA (2005) and OEHHA (2012) note that conservative assumptions used in a risk assessment are intended to ensure that the estimated risks do not underestimate the actual risks. Therefore, the estimated risks do not necessarily represent actual risks experienced by populations at or near a site. The use of conservative assumptions tends to produce upper-bound estimates of risk and usually overestimate exposure and thus risk. For this resident-based risk assessment, the following conservative assumptions were used:

## 7. Conclusions

- To determine the MER for the unmitigated scenario, as reported in Table 2, it was assumed that children and/or adults stood outside of their residence for 24 hours per day, 350 days/year for 9 years (children) or 70 years (adults). In reality, it is likely that children and adults typically will spend just over one hour per day outdoors at their residences (CARB, 1991), which would result in a lower estimated risk value.
- For the unmitigated scenario, it was assumed that children and adults remained at home one hundred percent of the time (i.e., fraction of time at home of 1.0). In reality, it is likely that children and adults would only spend a fraction of time at home (FAH), which would result in a lower estimated risk value. OEHHA (2012) recommends the following FAH values for estimating health risk values:

| Age Range | $\underline{\text { FAH }}$ |
| :--- | :--- |
| Third Trimester - | 0.85 |
| 2-16 | 0.72 |
| $16-70$ | 0.73 |

- The calculated risk for pregnant women and children from 0-2 years was multiplied by a factor of 10 (age sensitivity factor) and the calculated risk for children from 2-16 years was multiplied by a factor of 3 to account for early life exposure and uncertainty in child vs. adult exposure impacts. Thus, the estimated risks are conservative.

Nevertheless, because the carcinogenic risks for the child scenario and maximum annual $\mathrm{PM}_{2.5}$ concentrations are predicted to be above the significance thresholds, mitigation measures are warranted. The following mitigation measures are proposed:

- During the construction phase, the construction contractor shall be required to use equipment retrofitted with Level 3 Diesel Particulate Filters for construction equipment with engines rated 50 horsepower and greater. Level 3 Diesel Particulate Filters are capable of reducing particulate matter emissions by 85 percent (SCAQMD, 2009). A list of construction equipment by type and model year shall be maintained by the construction contractor onsite. The construction contractor shall ensure that all construction equipment is properly serviced and maintained to the manufacturer's standards to reduce operational emissions, and shall limit nonessential idling of construction equipment to no more than five consecutive minutes or less in compliance with California Air Resources Board's Rule 2449. Prior to issuance of any construction permits, the construction contractor shall submit a copy of construction equipment $\log$ to the City of Berkeley Department of Planning and Development for verification of this requirement. The City of Berkeley Building and Safety Division Official or their designee shall verify compliance that these measures have been implemented during normal construction site inspections.

The modeled average daily emission rates for the construction scenario with mitigation are summarized in Table 3.

Table 3 Construction Activity - Mitigated Scenario

| Parameter - Year | On-site Emissions (lbs/day) | Total Off-site Emissions (lbs/day) |
| :---: | :---: | :---: |
| DPM - 2015 | 0.37 | 0.16 |
| DPM -2016 | 0.68 | 0.06 |
| PM $_{2.5}-2015$ | 0.74 | 0.36 |
| $\mathrm{PM}_{2.5}-2016$ | 0.67 | 0.34 |

Mitigation includes Level 3 Diesel Particulate Filters for equipment 50 HP or greater and BAAQMD's Best Management Practices (BMPs) for Fugitive Dust. Presented emission rates are average daily emissions.
Source: CalEEMod 2013.2.2.

Assuming a resident or child would spend only a fraction of time at home ( 0.73 for the adult exposure scenario and 0.75 for the child scenario; OEHHA, 2012), the mitigated risk values were calculated and results are summarized in Table 4. The results indicate that with mitigation, the excess cancer risk for the adult and child exposure scenarios would be less than the threshold values for off-site receptors. Additionally, the $\mathrm{PM}_{2.5}$ annual concentrations would be below the significance threshold with mitigation for all receptor types. Therefore, with the mitigation measures described above, the Project would have a less than significant impact with respect to excess cancer risk, chronic non-hazard impacts, and $\mathrm{PM}_{2.5}$ emissions for off-site sensitive receptors during the construction period.

Table 4 Health Risk Assessment Results - Mitigated Scenario

| Receptor | Cancer Risk <br> (per million) | Chronic Hazard Index |
| :--- | :---: | :---: | :---: | | $\mathbf{P M}_{2.5}$ <br> $\left(\boldsymbol{\mu g / \mathbf { m } ^ { 3 } )}\right.$ |
| :---: |
| Adult Resident |
| Child Resident |
| Berkeley City College Adult Student/Staff |
| Berkeley High School Student |
| Berkeley High School Staff |
| BAAQMD Threshold |
| Exceeds Threshold |

Mitigation includes Level 3 Diesel Particulate Filters for equipment 50 HP or greater.
Sources: (Lakes AERMOD View, 8.8.1, 2014).

## 7. Conclusions

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## 8. References

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## 8. References

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## Appendix A. Emission Rate Calculations

## Appendix

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## Construction Emissions - DPM and PM2.5 <br> Input to ISCST3 Model

| Onsite Construction Emissions |  | DPM ${ }^{1}$ | PM ${ }_{25}{ }^{2}$ |
| :---: | :---: | :---: | :---: |
| 2015 Onsite Emissions | Average Daily Emissions (lbs/day) | 1.97 | 2.29 |
|  | Average Daily Emissions (lbs/hr) | $2.46 \mathrm{E}-01$ | $2.86 \mathrm{E}-01$ |
|  | Emission Rate (g/s) | $3.10 \mathrm{E}-02$ | $3.60 \mathrm{E}-02$ |
| 2016 Onsite Emissions | Average Daily Emissions (lbs/day) | 2.90 | 2.83 |
|  | Average Daily Emissions (lbs/hr) | $3.62 \mathrm{E}-01$ | $3.53 \mathrm{E}-01$ |
|  | Emission Rate (g/s) | $4.56 \mathrm{E}-02$ | $4.45 \mathrm{E}-02$ |

Note: Onsite emissions assumed to be evenly distributed over entire construction area.

| Offsite Construction Emissions |  |  | $\mathbf{D P M}^{\mathbf{1}}$ |
| :---: | :---: | :---: | :---: |
| 2015 Offsite | Haul Length Daily Emissions (lbs/day) | 0.16 | $\mathbf{P M}_{2.5}{ }^{\mathbf{2}}$ |
| Emissions | Hauling Emissions w/in $1,000 \mathrm{ft}(\mathrm{lbs} / \text { day })^{3}$ | $2.06 \mathrm{E}-03$ | $4.63 \mathrm{E}-03$ |
|  | Emission Rate (lbs/hr) | $2.57 \mathrm{E}-04$ | $5.79 \mathrm{E}-04$ |
|  | Emission Rate $(\mathrm{g} / \mathrm{s})$ | $3.24 \mathrm{E}-05$ | $7.29 \mathrm{E}-05$ |
| 2016 Offsite | Haul Length Daily Emissions $(\mathrm{lbs} /$ day $)$ | 0.06 | 0.34 |
| Emissions | Hauling Emissions w/in $1,000 \mathrm{ft}(\mathrm{lbs} / \text { day })^{3}$ | $8.27 \mathrm{E}-04$ | $4.37 \mathrm{E}-03$ |
|  | Emission Rate $(\mathrm{lbs} / \mathrm{hr})$ | $1.03 \mathrm{E}-04$ | $5.46 \mathrm{E}-04$ |
|  | Emission Rate $(\mathrm{g} / \mathrm{s})$ | $1.30 \mathrm{E}-05$ | $6.88 \mathrm{E}-05$ |

Note: Offsite emissions evenly distributed over 38 modeled volume sources.

Hours per work day (7:00 AM to 4:00 PM, 1-hour lunch break)

| 8 |
| :---: |


| Year | Total calendar days per year | Scalar $^{4}$ |
| :---: | :---: | :---: |
| 2015 | 44 | 0.12 |
| 2016 | 333 | 0.91 |

Default Hauling Length (miles)
Haul Length within $1,000 \mathrm{ft}$ of Site (mile)

| 20 |
| :---: |
| 0.26 |

${ }^{1}$ DPM emissions taken as $\mathrm{PM}_{10}$ exhaust emissions from CalEEMod average daily emissions.
${ }^{2} \mathrm{PM}_{2.5}$ emissions taken as total $\mathrm{PM}_{2.5}$ (exhaust and fugitive dust) emissions from CalEEMod average daily emissions.
${ }^{3}$ Emissions from CalEEMod offsite average daily emissions, which is based on haul truck trips of 20 miles
(model default) to evaluate emissions from 0.26 mile route within 1,000 feet of project site.
${ }^{4}$ Scalar for days per year is the fraction of construction days per calendar year ( 365 days).
Number of construction days is 32 in 2015 and 238 in 2016, due to no operations occuring on the weekends.
This is accounted for in the ISCST3 model using SHRDOW module.

# Construction Emissions - DPM and PM2.5 <br> Input to ISCST3 Model <br> with Mitigation (Level 3 DPF) 

| Onsite Construction Emissions - Mitigated |  | DPM ${ }^{1}$ | PM ${ }_{2.5}{ }^{2}$ |
| :---: | :---: | :---: | :---: |
| 2015 Onsite Emissions | Average Daily Emissions (lbs/day) | 0.37 | 0.74 |
|  | Average Daily Emissions (lbs/hr) | $4.63 \mathrm{E}-02$ | $9.27 \mathrm{E}-02$ |
|  | Emission Rate (g/s) | 5.84E-03 | $1.17 \mathrm{E}-02$ |
| 2016 Onsite Emissions | Average Daily Emissions (lbs/day) | 0.68 | 0.67 |
|  | Average Daily Emissions (lbs/hr) | $8.46 \mathrm{E}-02$ | $8.33 \mathrm{E}-02$ |
|  | Emission Rate (g/s) | $1.07 \mathrm{E}-02$ | $1.05 \mathrm{E}-02$ |

Note: Onsite emissions assumed to be evenly distributed over entire construction area.

| Offsite Construction Emissions - Mitigated |  | DPM $^{\mathbf{1}}$ | $\mathbf{P M}_{\mathbf{2 . 5}}{ }^{\mathbf{2}}$ |
| :---: | :---: | :---: | :---: |
| 2015 Offsite | Haul Length Daily Emissions (lbs/day) | 0.16 | 0.36 |
| Emissions | Hauling Emissions w/in $1,000 \mathrm{ft}(\mathrm{lbs} / \mathrm{day})^{3}$ | $2.06 \mathrm{E}-03$ | $4.63 \mathrm{E}-03$ |
|  | Emission Rate $(\mathrm{lbs} / \mathrm{hr})$ | $2.57 \mathrm{E}-04$ | $5.79 \mathrm{E}-04$ |
|  | Emission Rate $(\mathrm{g} / \mathrm{s})$ | $3.24 \mathrm{E}-05$ | $7.29 \mathrm{E}-05$ |
| 2016 Offsite | Haul Length Daily Emissions (lbs/day) | 0.06 | 0.34 |
| Emissions | Hauling Emissions w/in $1,000 \mathrm{ft}(\mathrm{lbs} / \mathrm{day})^{3}$ | $8.27 \mathrm{E}-04$ | $4.37 \mathrm{E}-03$ |
|  | Emission Rate $(\mathrm{lbs} / \mathrm{hr})$ | $1.03 \mathrm{E}-04$ | $5.46 \mathrm{E}-04$ |
|  | Emission Rate $(\mathrm{g} / \mathrm{s})$ | $1.30 \mathrm{E}-05$ | $6.88 \mathrm{E}-05$ |

Note: Offsite emissions evenly distributed over 38 modeled volume sources.

Hours per work day (7:00 AM to 4:00 PM, 1-hour lunch break)

| 8 |
| :---: |


| Year | Total calendar days per year | Scalar $^{4}$ |
| :---: | :---: | :---: |
| 2015 | 44 | 0.12 |
| 2016 | 333 | 0.91 |

Default Hauling Length (miles)
Haul Length within $1,000 \mathrm{ft}$ of Site (mile)

| 20 |
| :---: |
| 0.26 |

${ }^{1}$ DPM emissions taken as $\mathrm{PM}_{10}$ exhaust emissions from CalEEMod average daily emissions.
${ }^{2} \mathrm{PM}_{2.5}$ emissions taken as total $\mathrm{PM}_{2.5}$ (exhaust and fugitive dust) emissions from CalEEMod average daily emissions.
${ }^{3}$ Emissions from CalEEMod offsite average daily emissions, which is based on haul truck trips of 20 miles
(model default) to evaluate emissions from 0.26 mile route within 1,000 feet of project site.
${ }^{4}$ Scalar for days per year is the fraction of construction days per calendar year ( 365 days).
Number of construction days is 32 in 2015 and 238 in 2016, due to no operations occuring on the weekends.
This is accounted for in the ISCST3 model using SHRDOW module.


## BAAQMD Meteorological Site

Name: UC Richmond
Site ID: 2950
Start Date: 7/1/1999
End Date: current

| 2005 | metdata2950-05met.zip |
| :--- | :--- |
| 2004 | metdata2950-04met.zip |
| 2003 | $\underline{\text { metdata2950-03met.zip }}$ |
| 2002 | $\underline{\text { metdata2950-02met.zip }}$ |
| 2001 | $\underline{\text { metdata2950-01met.zip }}$ |
| 2000 | $\underline{\text { metdata2950-00met.zip }}$ |

## Files for Downloading

Operator: BAAQMD
Latitude: 37.9148
Longitude: 122.3379
Elevation: 1 m
Wind Height: 10 m
UTM - East: 558.194
UTM - North: 4196.566
County: Contra Costa
Sensors: ws,wd,temp solar insolation

Note: An "A" instead of a filename for any given year in the ASCll column signifies the data are missing. An "A" in the ISCST3 columns indicates the data are either missing or do not meet the EPA $90 \%$ data capture rate required for regulatory modeling applications.

## Appendix B. ISCST3 Model Output Files

## Appendix

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```
*** ISCST3 - VERSION 02035 *** *** Center St Garage
*** Construction HRA
**MODELOPTS:
CONC
URBAN FLAT FLGPOL DFAULT
13:19:24
```

```
*** MODEL SETUP OPTIONS SUMMARY
```

*** MODEL SETUP OPTIONS SUMMARY
***

```
***
```

**Intermediate Terrain Processing is Selected
**Model Is Setup For Calculation of Average CONCentration Values.
-_ SCAVENGING/DEPOSITION LOGIC -_
**Model Uses NO DRY DEPLETION. DDPLETE $=\mathrm{F}$
**Model Uses NO WET DEPLETION. WDPLETE = F
**NO WET SCAVENGING Data Provided.
**NO GAS DRY DEPOSITION Data Provided.
**Model Does NOT Use GRIDDED TERRAIN Data for Depletion Calculations
**Model Uses URBAN Dispersion.
**Model Uses Regulatory DEFAULT Options:

1. Final Plume Rise.
2. Stack-tip Downwash.
3. Buoyancy-induced Dispersion.
4. Use Calms Processing Routine
5. Not Use Missing Data Processing Routine.
6. Default Wind Profile Exponents.
7. Default Vertical Potential Temperature Gradients.
8. "Upper Bound" Values for Supersquat Buildings.
9. No Exponential Decay for URBAN/Non-SO2
**Model Assumes Receptors on FLAT Terrain.
**Model Accepts FLAGPOLE Receptor Heights.
**Model Calculates ANNUAL Averages Only
**This Run Includes: 39 Source(s); 2 Source Group(s); and 109 Receptor(s)
**The Model Assumes A Pollutant Type of: OTHER
**Model Set To Continue RUNning After the Setup Testing.
**Output Options Selected:
Model Outputs Tables of ANNUAL Averages by Receptor
Model Outputs External File(s) of High Values for Plotting (PLOTFILE Keyword)
**NOTE: The Following Flags May Appear Following CONC Values: c for Calm Hours
m for Missing Hours
b for Both Calm and Missing Hours

**Input Runstream File: CenterSt.INP
**Output Print File: CenterSt.OUT
**Detailed Error/Message File: CenterSt.err

|  | NUMBER | EMISSION RATE |  |  | BASE | RELEASE | INIT. | INIT. | EMISSION RATE |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SOURCE | PART. | (GRAMS / SEC) | X | Y | ELEV. | HEIGHT | SY | SZ | SCALAR VARY |
| ID | CATS. |  | (METERS) | (METERS) | (METERS) | (METERS) | (METERS) | (METERS) | BY |



## *** AREAPOLY SOURCE DATA ***



```
*** ISCST3 - VERSION 02035 *** *** Center St Garage
*** Construction HRA
*** 01/29/15
*** 13:19:2
**MODELOPTs
CONC
URBAN FLAT FLGPOL DFAULT
```

*** SOURCE IDs DEFINING SOURCE GROUPS ***

L0000115, L0000116, L0000117, L0000118, L0000119, L0000120, L0000121, L0000122, L0000123, L0000124, L0000125, L0000126, L0000127, L0000128, L0000129, L0000130, L0000131, L0000132, L0000133, L0000134, L0000135, L0000136, L0000137, L0000138, L0000139, L0000140, L0000141, L0000142, L0000143, L0000144, L0000145, L0000146, L0000147, L0000148, L0000149, L0000150, L0000151, L0000152,


|  |  |  |  |  |  | SEASO | = SUMMER; | DAY | OF WEEK = | SUNDA |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | . $0000 \mathrm{E}+00$ | 2 | . $0000 \mathrm{E}+00$ | 3 | . $0000 \mathrm{E}+00$ | 4 | . $0000 \mathrm{E}+00$ | 5 | . $0000 \mathrm{E}+00$ | 6 | . $0000 \mathrm{E}+00$ | 7 | . $0000 \mathrm{E}+00$ | 8 | . $0000 \mathrm{E}+00$ |
| 9 | . $0000 \mathrm{E}+00$ | 10 | . $0000 \mathrm{E}+00$ | 11 | . $0000 \mathrm{E}+00$ | 12 | . $0000 \mathrm{E}+00$ | 13 | . $0000 \mathrm{E}+00$ | 14 | . $0000 \mathrm{E}+00$ | 15 | . $0000 \mathrm{E}+00$ | 16 | . $0000 \mathrm{E}+00$ |
| 17 | . $0000 \mathrm{E}+00$ | 18 | . $0000 \mathrm{E}+00$ | 19 | . $0000 \mathrm{E}+00$ | 20 | . $0000 \mathrm{E}+00$ | 21 | . $0000 \mathrm{E}+00$ | 22 | . $0000 \mathrm{E}+00$ | 23 | . $0000 \mathrm{E}+00$ | 24 | . $0000 \mathrm{E}+00$ |
|  |  |  |  |  |  | SEASO | = FALL ; | DAY | OF WEEK = | SUNDAY |  |  |  |  |  |
| 1 | . $0000 \mathrm{E}+00$ | 2 | . $0000 \mathrm{E}+00$ | 3 | . $0000 \mathrm{E}+00$ | 4 | . $0000 \mathrm{E}+00$ | 5 | . $0000 \mathrm{E}+00$ | 6 | . $0000 \mathrm{E}+00$ | 7 | . $0000 \mathrm{E}+00$ | 8 | . $0000 \mathrm{E}+00$ |
| 9 | . $0000 \mathrm{E}+00$ | 10 | . $0000 \mathrm{E}+00$ | 11 | . $0000 \mathrm{E}+00$ | 12 | . $0000 \mathrm{E}+00$ | 13 | . $0000 \mathrm{E}+00$ | 14 | . $0000 \mathrm{E}+00$ | 15 | . $0000 \mathrm{E}+00$ | 16 | . $0000 \mathrm{E}+00$ |
| 17 | . $0000 \mathrm{E}+00$ | 18 | . $0000 \mathrm{E}+00$ | 19 | . $0000 \mathrm{E}+00$ | 20 | . $0000 \mathrm{E}+00$ | 21 | . $0000 \mathrm{E}+00$ | 22 | . $0000 \mathrm{E}+00$ | 23 | . $0000 \mathrm{E}+00$ | 24 | . $0000 \mathrm{E}+00$ |

SOURCE ID $=$ L0000115 through L0000152; SOURCE TYPE = VOLUME

| HOUR | SCALAR | HOUR | SCALAR | HOUR | SCALAR | HOUR | SCALAR | HOUR | SCALAR | HOUR | SCALAR | HOUR | SCALAR | HOUR | SCALAR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | - - - - |  | - - - - - | SEASON | N = WINTER; | DAY | OF WEEK = | WEEK | AY - - - |  | - - - |  |  |
| 1 | . $0000 \mathrm{E}+00$ | 2 | . $0000 \mathrm{E}+00$ | 3 | . $0000 \mathrm{E}+00$ | 4 | $.0000 \mathrm{E}+00$ | 5 | . $0000 \mathrm{E}+00$ | 6 | . $0000 \mathrm{E}+00$ | 7 | . $0000 \mathrm{E}+00$ | 8 | . $1000 \mathrm{E}+01$ |
| 9 | $.1000 \mathrm{E}+01$ | 10 | . $1000 \mathrm{E}+01$ | 11 | . $1000 \mathrm{E}+01$ | 12 | $.1000 \mathrm{E}+01$ | 13 | $.0000 \mathrm{E}+00$ | 14 | $.1000 \mathrm{E}+01$ | 15 | . $1000 \mathrm{E}+01$ | 16 | . $1000 \mathrm{E}+01$ |
| 17 | . $0000 \mathrm{E}+00$ | 18 | . $0000 \mathrm{E}+00$ | 19 | . $0000 \mathrm{E}+00$ | 20 | . $0000 \mathrm{E}+00$ | 21 | . $0000 \mathrm{E}+00$ | 22 | $.0000 \mathrm{E}+00$ | 23 | $.0000 \mathrm{E}+00$ | 24 | . $0000 \mathrm{E}+00$ |
|  |  |  |  |  |  | SEASON | $N=$ SPRING; | DAY | OF WEEK = | WEEKD |  |  |  |  |  |
| 1 | . $0000 \mathrm{E}+00$ | 2 | . $0000 \mathrm{E}+00$ | 3 | . $0000 \mathrm{E}+00$ | 4 | $.0000 \mathrm{E}+00$ | 5 | . $0000 \mathrm{E}+00$ | 6 | $.0000 \mathrm{E}+00$ | 7 | . $0000 \mathrm{E}+00$ | 8 | . $1000 \mathrm{E}+01$ |
| 9 | . $1000 \mathrm{E}+01$ | 10 | . $1000 \mathrm{E}+01$ | 11 | . $1000 \mathrm{E}+01$ | 12 | $.1000 \mathrm{E}+01$ | 13 | $.0000 \mathrm{E}+00$ | 14 | $.1000 \mathrm{E}+01$ | 15 | . $1000 \mathrm{E}+01$ | 16 | . $1000 \mathrm{E}+01$ |
| 17 | . $0000 \mathrm{E}+00$ | 18 | . $0000 \mathrm{E}+00$ | 19 | . $0000 \mathrm{E}+00$ | 20 | . $0000 \mathrm{E}+00$ | 21 | $.0000 \mathrm{E}+00$ | 22 | $.0000 \mathrm{E}+00$ | 23 | . $0000 \mathrm{E}+00$ | 24 | . $0000 \mathrm{E}+00$ |
|  |  |  |  |  |  | SEASON | N = SUMMER; | DAY | OF WEEK = | WEEKD |  |  |  |  |  |
| 1 | . $0000 \mathrm{E}+00$ | 2 | . $0000 \mathrm{E}+00$ | 3 | . $0000 \mathrm{E}+00$ | 4 | $.0000 \mathrm{E}+00$ | 5 | $.0000 \mathrm{E}+00$ | 6 | . $0000 \mathrm{E}+00$ | 7 | $.0000 \mathrm{E}+00$ | 8 | . $1000 \mathrm{E}+01$ |
| 9 | . $1000 \mathrm{E}+01$ | 10 | . $1000 \mathrm{E}+01$ | 11 | . $1000 \mathrm{E}+01$ | 12 | . $1000 \mathrm{E}+01$ | 13 | . $0000 \mathrm{E}+00$ | 14 | . $1000 \mathrm{E}+01$ | 15 | . $1000 \mathrm{E}+01$ | 16 | . $1000 \mathrm{E}+01$ |
| 17 | . $0000 \mathrm{E}+00$ | 18 | . $0000 \mathrm{E}+00$ | 19 | . $0000 \mathrm{E}+00$ | 20 | . $0000 \mathrm{E}+00$ | 21 | . $0000 \mathrm{E}+00$ | 22 | $.0000 \mathrm{E}+00$ | 23 | . $0000 \mathrm{E}+00$ | 24 | . $0000 \mathrm{E}+00$ |
|  |  |  |  |  |  | SEASON | $N=$ FALL ; | DAY | OF WEEK = | WEEKD |  |  |  |  |  |
| 1 | . $0000 \mathrm{E}+00$ | 2 | . $0000 \mathrm{E}+00$ | 3 | . $0000 \mathrm{E}+00$ | 4 | $.0000 \mathrm{E}+00$ | 5 | $.0000 \mathrm{E}+00$ | 6 | $.0000 \mathrm{E}+00$ | 7 | $.0000 \mathrm{E}+00$ | 8 | . $1000 \mathrm{E}+01$ |
| 9 | . $1000 \mathrm{E}+01$ | 10 | . $1000 \mathrm{E}+01$ | 11 | . $1000 \mathrm{E}+01$ | 12 | . $1000 \mathrm{E}+01$ | 13 | . $0000 \mathrm{E}+00$ | 14 | $.1000 \mathrm{E}+01$ | 15 | . $1000 \mathrm{E}+01$ | 16 | . $1000 \mathrm{E}+01$ |
| 17 | . $0000 \mathrm{E}+00$ | 18 | . $0000 \mathrm{E}+00$ | 19 | . $0000 \mathrm{E}+00$ | 20 | . $0000 \mathrm{E}+00$ | 21 | . $0000 \mathrm{E}+00$ | 22 | . $0000 \mathrm{E}+00$ | 23 | . $0000 \mathrm{E}+00$ | 24 | . $0000 \mathrm{E}+00$ |
|  |  |  |  |  |  | SEASON | N = WINTER; | DAY | OF WEEK = | SATURD | AY |  |  |  |  |
| 1 | . $0000 \mathrm{E}+00$ | 2 | . $0000 \mathrm{E}+00$ | 3 | . $0000 \mathrm{E}+00$ | 4 | $.0000 \mathrm{E}+00$ | 5 | . $0000 \mathrm{E}+00$ | 6 | $.0000 \mathrm{E}+00$ | 7 | . $0000 \mathrm{E}+00$ | 8 | . $0000 \mathrm{E}+00$ |
| 9 | . $0000 \mathrm{E}+00$ | 10 | . $0000 \mathrm{E}+00$ | 11 | . $0000 \mathrm{E}+00$ | 12 | $.0000 \mathrm{E}+00$ | 13 | $.0000 \mathrm{E}+00$ | 14 | $.0000 \mathrm{E}+00$ | 15 | . $0000 \mathrm{E}+00$ | 16 | . $0000 \mathrm{E}+00$ |
| 17 | . $0000 \mathrm{E}+00$ | 18 | . $0000 \mathrm{E}+00$ | 19 | . $0000 \mathrm{E}+00$ | 20 | . $0000 \mathrm{E}+00$ | 21 | . $0000 \mathrm{E}+00$ | 22 | . $0000 \mathrm{E}+00$ | 23 | . $0000 \mathrm{E}+00$ | 24 | . $0000 \mathrm{E}+00$ |
|  |  |  |  |  |  | SEASON | $\mathrm{N}=$ SPRING; | DAY | OF WEEK = | SATUR |  |  |  |  |  |
| 1 | . $0000 \mathrm{E}+00$ | 2 | . $0000 \mathrm{E}+00$ | 3 | . $0000 \mathrm{E}+00$ | 4 | . $0000 \mathrm{E}+00$ | 5 | . $0000 \mathrm{E}+00$ | 6 | $.0000 \mathrm{E}+00$ | 7 | . $0000 \mathrm{E}+00$ | 8 | . $0000 \mathrm{E}+00$ |
| 9 | . $0000 \mathrm{E}+00$ | 10 | . $0000 \mathrm{E}+00$ | 11 | . $0000 \mathrm{E}+00$ | 12 | . $0000 \mathrm{E}+00$ | 13 | . $0000 \mathrm{E}+00$ | 14 | . $0000 \mathrm{E}+00$ | 15 | . $0000 \mathrm{E}+00$ | 16 | . $0000 \mathrm{E}+00$ |
| 17 | . $0000 \mathrm{E}+00$ | 18 | . $0000 \mathrm{E}+00$ | 19 | . $0000 \mathrm{E}+00$ | 20 | . $0000 \mathrm{E}+00$ | 21 | . $0000 \mathrm{E}+00$ | 22 | . $0000 \mathrm{E}+00$ | 23 | $.0000 \mathrm{E}+00$ | 24 | . $0000 \mathrm{E}+00$ |
|  |  |  |  |  |  | SEASON | N = SUMMER; | DAY | OF WEEK = | SATURD |  |  |  |  |  |
| 1 | . $0000 \mathrm{E}+00$ | 2 | . $0000 \mathrm{E}+00$ | 3 | . $0000 \mathrm{E}+00$ | 4 | $.0000 \mathrm{E}+00$ | 5 | . $0000 \mathrm{E}+00$ | 6 | $.0000 \mathrm{E}+00$ | 7 | . $0000 \mathrm{E}+00$ | 8 | . $0000 \mathrm{E}+00$ |
| 9 | . $0000 \mathrm{E}+00$ | 10 | . $0000 \mathrm{E}+00$ | 11 | . $0000 \mathrm{E}+00$ | 12 | . $0000 \mathrm{E}+00$ | 13 | . $0000 \mathrm{E}+00$ | 14 | . $0000 \mathrm{E}+00$ | 15 | . $0000 \mathrm{E}+00$ | 16 | . $0000 \mathrm{E}+00$ |
| 17 | . $0000 \mathrm{E}+00$ | 18 | . $0000 \mathrm{E}+00$ | 19 | . $0000 \mathrm{E}+00$ | 20 | . $0000 \mathrm{E}+00$ | 21 | . $0000 \mathrm{E}+00$ | 22 | . $0000 \mathrm{E}+00$ | 23 | . $0000 \mathrm{E}+00$ | 24 | . $0000 \mathrm{E}+00$ |
|  |  |  |  |  |  | SEASON | $N=$ FALL ; | DAY | OF WEEK = | SATURD |  |  |  |  |  |
| 1 | . $0000 \mathrm{E}+00$ | 2 | . $0000 \mathrm{E}+00$ | 3 | . $0000 \mathrm{E}+00$ | 4 | $.0000 \mathrm{E}+00$ | 5 | . $0000 \mathrm{E}+00$ | 6 | $.0000 \mathrm{E}+00$ | 7 | . $0000 \mathrm{E}+00$ | 8 | . $0000 \mathrm{E}+00$ |
| 9 | . $0000 \mathrm{E}+00$ | 10 | . $0000 \mathrm{E}+00$ | 11 | . $0000 \mathrm{E}+00$ | 12 | $.0000 \mathrm{E}+00$ | 13 | $.0000 \mathrm{E}+00$ | 14 | $.0000 \mathrm{E}+00$ | 15 | . $0000 \mathrm{E}+00$ | 16 | . $0000 \mathrm{E}+00$ |
| 17 | . $0000 \mathrm{E}+00$ | 18 | . $0000 \mathrm{E}+00$ | 19 | . $0000 \mathrm{E}+00$ | 20 | . $0000 \mathrm{E}+00$ | 21 | . $0000 \mathrm{E}+00$ | 22 | $.0000 \mathrm{E}+00$ | 23 | . $0000 \mathrm{E}+00$ | 24 | . $0000 \mathrm{E}+00$ |
|  |  |  |  |  |  | SEASON | N = WINTER; | DAY | OF WEEK = | SUNDAY |  |  |  |  |  |
| 1 | . $0000 \mathrm{E}+00$ | 2 | . $0000 \mathrm{E}+00$ | 3 | . $0000 \mathrm{E}+00$ | 4 | $.0000 \mathrm{E}+00$ | 5 | . $0000 \mathrm{E}+00$ | 6 | $.0000 \mathrm{E}+00$ | 7 | . $0000 \mathrm{E}+00$ | 8 | . $0000 \mathrm{E}+00$ |
| 9 | . $0000 \mathrm{E}+00$ | 10 | . $0000 \mathrm{E}+00$ | 11 | . $0000 \mathrm{E}+00$ | 12 | . $0000 \mathrm{E}+00$ | 13 | . $0000 \mathrm{E}+00$ | 14 | . $0000 \mathrm{E}+00$ | 15 | . $0000 \mathrm{E}+00$ | 16 | . $0000 \mathrm{E}+00$ |
| 17 | . $0000 \mathrm{E}+00$ | 18 | . $0000 \mathrm{E}+00$ | 19 | . $0000 \mathrm{E}+00$ | 20 | . $0000 \mathrm{E}+00$ | 21 | $.0000 \mathrm{E}+00$ | 22 | $.0000 \mathrm{E}+00$ | 23 | $.0000 \mathrm{E}+00$ | 24 | . $0000 \mathrm{E}+00$ |
|  |  |  |  |  |  | SEASON | $\mathrm{N}=$ SPRING; | DAY | OF WEEK = | SUNDAY |  |  |  |  |  |
| 1 | . $0000 \mathrm{E}+00$ | 2 | . $0000 \mathrm{E}+00$ | 3 | . $0000 \mathrm{E}+00$ | 4 | . $0000 \mathrm{E}+00$ | 5 | . $0000 \mathrm{E}+00$ | 6 | $.0000 \mathrm{E}+00$ | 7 | . $0000 \mathrm{E}+00$ | 8 | . $0000 \mathrm{E}+00$ |
| 9 | . $0000 \mathrm{E}+00$ | 10 | . $0000 \mathrm{E}+00$ | 11 | . $0000 \mathrm{E}+00$ | 12 | . $0000 \mathrm{E}+00$ | 13 | . $0000 \mathrm{E}+00$ | 14 | . $0000 \mathrm{E}+00$ | 15 | . $0000 \mathrm{E}+00$ | 16 | . $0000 \mathrm{E}+00$ |
| 17 | $.0000 \mathrm{E}+00$ | 18 | . $0000 \mathrm{E}+00$ | 19 | . $0000 \mathrm{E}+00$ | 20 | . $0000 \mathrm{E}+00$ | 21 | . $0000 \mathrm{E}+00$ | 22 | . $0000 \mathrm{E}+00$ | 23 | $.0000 \mathrm{E}+00$ | 24 | . $0000 \mathrm{E}+00$ |


| 1 | . $0000 \mathrm{E}+00$ | 2 | . $0000 \mathrm{E}+00$ | 3 | . $0000 \mathrm{E}+00$ | 4 | . $0000 \mathrm{E}+00$ | 5 | . $0000 \mathrm{E}+00$ | 6 | . $0000 \mathrm{E}+00$ | 7 | . $0000 \mathrm{E}+00$ | 8 | . $0000 \mathrm{E}+00$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 9 | . $0000 \mathrm{E}+00$ | 10 | . $0000 \mathrm{E}+00$ | 11 | . $0000 \mathrm{E}+00$ | 12 | . $0000 \mathrm{E}+00$ | 13 | . $0000 \mathrm{E}+00$ | 14 | . $0000 \mathrm{E}+00$ | 15 | . $0000 \mathrm{E}+00$ | 16 | . $0000 \mathrm{E}+00$ |
| 17 | . $0000 \mathrm{E}+00$ | 18 | . $0000 \mathrm{E}+00$ | 19 | . $0000 \mathrm{E}+00$ | 20 | . $0000 \mathrm{E}+00$ | 21 | . $0000 \mathrm{E}+00$ | 22 | . $0000 \mathrm{E}+00$ | 23 | . $0000 \mathrm{E}+00$ | 24 | . $0000 \mathrm{E}+00$ |
|  |  |  |  |  |  | SEASON = FALL ; DAY OF WEEK = SUNDAY |  |  |  |  |  |  |  |  |  |
| 1 | . $0000 \mathrm{E}+00$ | 2 | . $0000 \mathrm{E}+00$ | 3 | . $0000 \mathrm{E}+00$ | 4 | . $0000 \mathrm{E}+00$ | 5 | . $0000 \mathrm{E}+00$ | 6 | . $0000 \mathrm{E}+00$ | 7 | . $0000 \mathrm{E}+00$ | 8 | . $0000 \mathrm{E}+00$ |
| 9 | . $0000 \mathrm{E}+00$ | 10 | . $0000 \mathrm{E}+00$ | 11 | . $0000 \mathrm{E}+00$ | 12 | . $0000 \mathrm{E}+00$ | 13 | . $0000 \mathrm{E}+00$ | 14 | . $0000 \mathrm{E}+00$ | 15 | . $0000 \mathrm{E}+00$ | 16 | . $0000 \mathrm{E}+00$ |
| 17 | . $0000 \mathrm{E}+00$ | 18 | . $0000 \mathrm{E}+00$ | 19 | . $0000 \mathrm{E}+00$ | 20 | . $0000 \mathrm{E}+00$ | 21 | . $0000 \mathrm{E}+00$ | 22 | . $0000 \mathrm{E}+00$ | 23 | . $0000 \mathrm{E}+00$ | 24 | . $0000 \mathrm{E}+00$ |


| ( 564245.5, 4191664.0, | 0.0, | 9.1); | ( 564253.2, | 4191666.0, | 0.0, | 9.1); |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ( 564263.6, 4191667.8, | 0.0, | 9.1); | ( 564284.6, | 4191701.0, | 0.0, | 9.1); |
| ( 564243.8, 4191673.0, | 0.0, | 9.1); | ( 564253.8, | 4191673.0, | 0.0, | 9.1); |
| ( 564263.8, 4191673.0, | 0.0, | 9.1); | ( 564273.8, | 4191673.0, | 0.0, | 9.1); |
| 564283.8, 4191673.0, | 0.0, | 9.1); | ( 564293.8, | 4191673.0, | 0.0, | 9.1); |
| 564303.8, 4191673.0, | 0.0, | 9.1); | ( 564243.8, | 4191683.0, | 0.0, | 9.1); |
| ( 564253.8, 4191683.0, | 0.0, | 9.1); | ( 564263.8, | 4191683.0, | 0.0, | 9.1); |
| 564273.8, 4191683.0, | 0.0, | 9.1); | ( 564283.8, | 4191683.0, | 0.0, | 9.1); |
| ( 564293.8, 4191683.0, | 0.0, | 9.1); | ( 564301.9, | 4191683.2, | 0.0, | 9.1); |
| ( 564243.8, 4191693.0, | 0.0, | 9.1); | ( 564253.8, | 4191693.0, | 0.0, | 9.1); |
| ( 564263.8, 4191693.0, | 0.0, | 9.1); | ( 564273.8, | 4191693.0, | 0.0, | 9.1); |
| ( 564283.8, 4191693.0, | 0.0, | 9.1); | ( 564293.8, | 4191693.0, | 0.0, | 9.1); |
| ( 564273.6, 4191700.2, | 0.0, | 9.1); | ( 564293.8, | 4191703.0, | 0.0, | 9.1); |
| ( 564238.7, 4191688.5, | 0.0, | 9.1); | ( 564162.2, | 4191714.0, | 0.0, | 9.1); |
| ( 564172.2, 4191714.0, | 0.0, | 9.1); | ( 564182.2, | 4191716.5, | 0.0, | 9.1); |
| ( 564157.0, 4191718.2, | 0.0, | 9.1); | ( 564162.2, | 4191724.0, | 0.0, | 9.1); |
| ( 564172.2, 4191724.0, | 0.0, | 9.1); | ( 564182.2, | 4191724.0, | 0.0, | 9.1); |
| ( 564176.5, 4191729.2, | 0.0, | 9.1); | ( 564319.4, | 4191713.8, | 0.0, | 9.1); |
| ( 564329.4, 4191713.8, | 0.0, | 9.1); | ( 564319.4, | 4191723.8, | 0.0, | 9.1); |
| ( 564329.4, 4191723.8, | 0.0, | 9.1); | ( 564339.4, | 4191723.8, | 0.0, | 9.1); |
| ( 564319.4, 4191733.8, | 0.0, | 9.1); | ( 564329.4, | 4191733.8, | 0.0, | 9.1); |
| ( 564339.4, 4191733.8, | 0.0, | 9.1); | ( 564319.4, | 4191743.8, | 0.0, | 9.1); |
| ( 564329.4, 4191743.8, | 0.0, | 9.1); | ( 564339.4, | 4191743.8, | 0.0, | 9.1); |
| ( 564319.4, 4191750.5, | 0.0, | 9.1); | ( 564329.4, | 4191753.8, | 0.0, | 9.1); |
| ( 564339.4, 4191753.8, | 0.0, | 9.1); | ( 564312.7, | 4191749.5, | 0.0, | 9.1); |
| ( 564315.1, 4191728.0, | 0.0, | 9.1); | ( 564172.8, | 4191830.5, | 0.0, | 6.1); |
| ( 564172.8, 4191817.8, | 0.0, | 6.1); | ( 564174.1, | 4191808.2, | 0.0, | 6.1); |
| ( 564175.9, 4191796.8, | 0.0, | 6.1); | ( 563882.5, | 4191825.5, | 0.0, | 6.1); |
| ( 563892.5, 4191825.5, | 0.0, | 6.1); | ( 563902.5, | 4191825.5, | 0.0, | 6.1); |
| ( 563912.5, 4191825.5, | 0.0, | 6.1); | ( 563922.5, | 4191825.5, | 0.0, | 6.1); |
| ( 563882.5, 4191835.5, | 0.0, | 6.1); | ( 563892.5, | 4191835.5, | 0.0, | 6.1); |
| ( 563902.5, 4191835.5, | 0.0, | 6.1); | ( 563912.5, | 4191835.5, | 0.0, | 6.1); |
| ( 563922.5, 4191835.5, | 0.0, | 6.1); | ( 563882.5, | 4191845.5, | 0.0, | 6.1); |
| ( 563892.5, 4191845.5, | 0.0, | 6.1); | ( 563902.5, | 4191845.5, | 0.0, | 6.1); |
| ( 563912.5, 4191845.5, | 0.0, | 6.1); | ( 563922.5, | 4191845.5, | 0.0, | 6.1); |
| ( 563882.5, 4191855.5, | 0.0, | 6.1); | ( 563892.5, | 4191855.5, | 0.0, | 6.1); |
| ( 563902.5, 4191855.5, | 0.0, | 6.1); | ( 563912.5, | 4191855.5, | 0.0, | 6.1); |
| ( 563922.5, 4191855.5, | 0.0, | 6.1); | ( 563902.5, | 4191865.5, | 0.0, | 6.1); |
| ( 563912.5, 4191865.5, | 0.0, | 6.1); | ( 563922.5, | 4191865.5, | 0.0, | 6.1); |
| ( 563902.5, 4191875.5, | 0.0, | 6.1); | ( 563912.5, | 4191875.5, | 0.0, | 6.1); |
| ( 563922.5, 4191875.5, | 0.0, | 6.1); | ( 564003.8, | 4191730.5, | 0.0, | 1.5); |


| 563940.5, 4191484.2, | 0.0, | 1.5); | ( 563942.3, 4191469.0, | 0.0, | 1.5) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| ( 563945.3, 4191452.8, | 0.0, | 1.5); | ( 563893.9, 4191477.0, | 0.0, | 1.5) |
| ( 563889.6, 4191468.5, | 0.0, | 1.5); | ( 563890.8, 4191454.5, | 0.0, | 1.5) |
| ( 563945.9, 4191440.5, | 0.0, | 1.5) ; | ( 563916.2, 4191722.0, | 0.0, | 1.5) |
| ( 563904.2, 4191718.5, | 0.0, | 1.5); | ( 563894.5, 4191716.5, | 0.0, | 1.5) |
| ( 563883.6, 4191713.0, | 0.0, | 1.5); | ( 564138.4, 4191503.5, | 0.0, | 1.5) |
| ( 564143.2, 4191467.2, | 0.0, | 1.5); | ( 564146.9, 4191414.0, | 0.0, | 1.5) |
| ( 564093.0, 4191495.8, | 0.0, | 1.5); | ( 564040.4, 4191490.3, | 0.0, | 1.5) |
| ( 563996.8, 4191484.2, | 0.0, | 1.5); | ( 564207.4, 4191622.0, | 0.0, | 1.5) |
| ( 564209.9, 4191608.0, | 0.0, | 1.5); | ( 564224.0, 4191624.5, | 0.0, | 1.5) |
| ( 564246.9, 4191632.5, | 0.0, | 1.5); | ( 564249.0, 4191623.5, | 0.0, | 1.5) |
| ( 564250.9, 4191612.3, | 0.0, | 1.5); | ( 564225.6, 4191616.5, | 0.0, | 1.5) |
| ( 564236.5, 4191626.0, | 0.0, | 1.5); | ( 564236.8, 4191609.2, | 0.0, | 1.5) |
| ( 564259.4, 4191623.3, | 0.0, | 1.5) |  |  |  |

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*** ISCST3 - VERSION 02035 *** *** Center St Garage
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*** Construction HRA

| $* * *$ | $01 / 29 / 15$ |
| :--- | :--- |
| $* * *$ | $13: 19: 24$ |
|  | PAGE 46 |

**MODELOPTS:
CONC
URBAN FLAT FLGPOL DFAULT
*** METEOROLOGICAL DAYS SELECTED FOR PROCESSING ***
(1=YES; 0=NO)


NOTE: METEOROLOGICAL DATA ACTUALLY PROCESSED WILL ALSO DEPEND ON WHAT IS INCLUDED IN THE DATA FILE
*** UPPER BOUND OF FIRST THROUGH FIFTH WIND SPEED CATEGORIES ***
(METERS/SEC)
1.54, 3.09, 5.14, 8.23, 10.80,
*** WIND PROFILE EXPONENTS ***

| STABILITY | WIND SPEED CATEGORY |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| CATEGORY | 1 | 2 | 3 | 4 | 5 | 6 |
| A | $.15000 \mathrm{E}+00$ | $.15000 \mathrm{E}+00$ | $.15000 \mathrm{E}+00$ | $.15000 \mathrm{E}+00$ | $.15000 \mathrm{E}+00$ | $.15000 \mathrm{E}+00$ |
| B | $.15000 \mathrm{E}+00$ | $.15000 \mathrm{E}+00$ | $.15000 \mathrm{E}+00$ | $.15000 \mathrm{E}+00$ | $.15000 \mathrm{E}+00$ | $.15000 \mathrm{E}+00$ |
| C | $.20000 \mathrm{E}+00$ | $.20000 \mathrm{E}+00$ | $.20000 \mathrm{E}+00$ | $.20000 \mathrm{E}+00$ | $.20000 \mathrm{E}+00$ | $.20000 \mathrm{E}+00$ |
| D | $.25000 \mathrm{E}+00$ | $.25000 \mathrm{E}+00$ | $.25000 \mathrm{E}+00$ | $.25000 \mathrm{E}+00$ | $.25000 \mathrm{E}+00$ | $.25000 \mathrm{E}+00$ |
| E | $.30000 \mathrm{E}+00$ | $.30000 \mathrm{E}+00$ | $.30000 \mathrm{E}+00$ | $.30000 \mathrm{E}+00$ | $.30000 \mathrm{E}+00$ | $.30000 \mathrm{E}+00$ |
| F | $.30000 \mathrm{E}+00$ | $.30000 \mathrm{E}+00$ | $.30000 \mathrm{E}+00$ | $.30000 \mathrm{E}+00$ | $.30000 \mathrm{E}+00$ | $.30000 \mathrm{E}+00$ |

*** VERTICAL POTENTIAL TEMPERATURE GRADIENTS *** (DEGREES KELVIN PER METER)

| STABILITY |  |
| :--- | :---: |
| CATEGORY | 1 |
| A | $.00000 \mathrm{E}+00$ |
| B | $.00000 \mathrm{E}+00$ |
| C | $.00000 \mathrm{E}+00$ |
| D | $.00000 \mathrm{E}+00$ |
| E | $.20000 \mathrm{E}-01$ |
| F | $.35000 \mathrm{E}-01$ |


| WIND SPEED CATEGORY |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2 | 3 | 4 | 5 | 6 |  |  |  |  |
| $.00000 \mathrm{E}+00$ | $.00000 \mathrm{E}+00$ | $.00000 \mathrm{E}+00$ | $.00000 \mathrm{E}+00$ | $.00000 \mathrm{E}+00$ |  |  |  |  |
| $.00000 \mathrm{E}+00$ | $.00000 \mathrm{E}+00$ | $.00000 \mathrm{E}+00$ | $.00000 \mathrm{E}+00$ | $.00000 \mathrm{E}+00$ |  |  |  |  |
| $.00000 \mathrm{E}+00$ | $.00000 \mathrm{E}+00$ | $.00000 \mathrm{E}+00$ | $.00000 \mathrm{E}+00$ | $.00000 \mathrm{E}+00$ |  |  |  |  |
| $.00000 \mathrm{E}+00$ | $.00000 \mathrm{E}+00$ | $.00000 \mathrm{E}+00$ | $.00000 \mathrm{E}+00$ | $.00000 \mathrm{E}+00$ |  |  |  |  |
| $.20000 \mathrm{E}-01$ | $.20000 \mathrm{E}-01$ | $.20000 \mathrm{E}-01$ | $.20000 \mathrm{E}-01$ | $.20000 \mathrm{E}-01$ |  |  |  |  |
| $.35000 \mathrm{E}-01$ | $.35000 \mathrm{E}-01$ | $.35000 \mathrm{E}-01$ | $.35000 \mathrm{E}-01$ | $.35000 \mathrm{E}-01$ |  |  |  |  |

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*** ISCST3 - VERSION 02035 *** *** Center St Garage
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**MODELOPTs:

CONC
URBAN FLAT FLGPOL DFAULT
*** THE FIRST 24 HOURS OF METEOROLOGICAL DATA ***
ILE: C:\!METFI~1 \BAAQMD~1 \UCR033~1. ASC
FORMAT: (4I2,2F9.4,F6.1,I2,2F7.1,f9.4,f10.1,f8.4,i4,f7.2)
SURFACE STATION NO.: 2950 UPPER AIR STATION NO.: 2950

| NAME : UNKNOWN | NAME: UNKNOWN |
| :--- | :--- |
| YEAR: 2003 | YEAR: 2003 |



| 03 | 010101 | 157.1 | 1.00 | 279.9 | 6 | 300.0 | 300.0 | 0.0000 | 0.0 | 0.0000 | 0 | 0.00 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 03 | 010102 | 192.2 | 1.00 | 279.5 | 6 | 300.0 | 300.0 | 0.0000 | 0.0 | 0.0000 | 0 | 0.00 |
| 03 | 010103 | 182.4 | 1.07 | 279.3 | 5 | 300.0 | 300.0 | 0.0000 | 0.0 | 0.0000 | 0 | 0.00 |
| 03 | 010104 | 142.7 | 1.30 | 278.9 | 6 | 300.0 | 300.0 | 0.0000 | 0.0 | 0.0000 | 0 | 0.00 |
| 03 | 010105 | 167.5 | 1.16 | 278.5 | 5 | 300.0 | 300.0 | 0.0000 | 0.0 | 0.0000 | 0 | 0.00 |
| 03 | 010106 | 140.0 | 1.30 | 278.4 | 5 | 300.0 | 300.0 | 0.0000 | 0.0 | 0.0000 | 0 | 0.00 |
| 03 | 010107 | 141.0 | 1.21 | 278.9 | 6 | 300.0 | 300.0 | 0.0000 | 0.0 | 0.0000 | 0 | 0.00 |
| 03 | 010108 | 223.4 | 1.83 | 280.4 | 6 | 300.0 | 300.0 | 0.0000 | 0.0 | 0.0000 | 0 | 0.00 |
| 03 | 010109 | 228.8 | 1.21 | 281.7 | 5 | 300.0 | 300.0 | 0.0000 | 0.0 | 0.0000 | 0 | 0.00 |
| 03 | 010110 | 266.6 | 2.15 | 282.8 | 4 | 300.0 | 300.0 | 0.0000 | 0.0 | 0.0000 | 0 | 0.00 |
| 03 | 010111 | 251.1 | 2.06 | 284.0 | 3 | 300.0 | 300.0 | 0.0000 | 0.0 | 0.0000 | 0 | 0.00 |
| 03 | 010112 | 196.5 | 2.82 | 285.3 | 2 | 300.0 | 300.0 | 0.0000 | 0.0 | 0.0000 | 0 | 0.00 |
| 03 | 010113 | 194.7 | 3.62 | 286.0 | 3 | 300.0 | 300.0 | 0.0000 | 0.0 | 0.0000 | 0 | 0.00 |
| 03 | 010114 | 208.0 | 2.41 | 287.0 | 2 | 300.0 | 300.0 | 0.0000 | 0.0 | 0.0000 | 0 | 0.00 |
| 03 | 010115 | 216.8 | 2.24 | 286.9 | 2 | 300.0 | 300.0 | 0.0000 | 0.0 | 0.0000 | 0 | 0.00 |
| 03 | 010116 | 228.3 | 2.46 | 286.8 | 1 | 300.0 | 300.0 | 0.0000 | 0.0 | 0.0000 | 0 | 0.00 |
| 03 | 010117 | 242.0 | 2.10 | 285.7 | 2 | 300.0 | 300.0 | 0.0000 | 0.0 | 0.0000 | 0 | 0.00 |
| 03 | 010118 | 236.2 | 1.92 | 285.1 | 3 | 300.0 | 300.0 | 0.0000 | 0.0 | 0.0000 | 0 | 0.00 |
| 03 | 010119 | 240.7 | 1.65 | 284.6 | 4 | 300.0 | 300.0 | 0.0000 | 0.0 | 0.0000 | 0 | 0.00 |
| 03 | 010120 | 272.2 | 2.06 | 284.7 | 5 | 300.0 | 300.0 | 0.0000 | 0.0 | 0.0000 | 0 | 0.00 |
| 03 | 010121 | 261.8 | 1.65 | 284.7 | 6 | 300.0 | 300.0 | 0.0000 | 0.0 | 0.0000 | 0 | 0.00 |
| 03 | 010122 | 285.9 | 1.79 | 284.5 | 6 | 300.0 | 300.0 | 0.0000 | 0.0 | 0.0000 | 0 | 0.00 |
| 03 | 010123 | 233.5 | 2.10 | 284.7 | 6 | 300.0 | 300.0 | 0.0000 | 0.0 | 0.0000 | 0 | 0.00 |
| 03 | 010124 | 177.0 | 1.83 | 284.1 | 6 | 300.0 | 300.0 | 0.0000 | 0.0 | 0.0000 | 0 | 0.00 |

*** NOTES: STABILITY CLASS 1=A, 2=B, 3=C, 4=D, 5=E AND 6=F.
FLOW VECTOR IS DIRECTION TOWARD WHICH WIND IS BLOWING.

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*** ISCST3 - VERSION 02035 *** *** Center St Garage
*** Construction HRA
*** 01/29/15
**MODELOPTs:
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CONC
URBAN FLAT FLGPOL DFAULT
*** THE ANNUAL ( 3 YRS) AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: 1 INCLUDING SOURCE (S): 1
*** DISCRETE CARTESIAN RECEPTOR POINTS ***
** CONC OF OTHER IN MICROGRAMS/M**3 **


| 563922.50 | 4191855.50 | 0.25775 | 563902.50 | 4191865.50 | 0.22839 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 563912.50 | 4191865.50 | 0.24630 | 563922.50 | 4191865.50 | 0.26552 |  |
| 563902.50 | 4191875.50 | 0.23528 | 563912.50 | 4191875.50 | 0.25258 |  |
| 563922.50 | 4191875.50 | 0.27081 | 564003.75 | 4191730.50 | 0.48987 |  |
| 563940.50 | 4191484.25 | 0.35143 | 563942.31 | 4191469.00 | 0.34418 |  |
| 563945.31 | 4191452.75 | 0.33843 | 563893.88 | 4191477.00 | 0.27346 |  |
| 563889.62 | 4191468.50 | 0.26339 | 563890.81 | 4191454.50 | 0.25786 |  |
| 563945.94 | 4191440.50 | 0.33050 | 563916.25 | 4191722.00 | 0.28184 |  |
| 563904.19 | 4191718.50 | 0.26534 | 563894.50 | 4191716.50 | 0.25229 |  |
| 563883.56 | 4191713.00 | 0.23894 | 564138.38 | 4191503.50 | 1.04967 | Berkeley High School Max |
| 564143.25 | 4191467.25 | 0.80791 | 564146.88 | 4191414.00 | 0.60225 |  |
| 564093.00 | 4191495.75 | 0.84617 | 564040.38 | 4191490.25 | 0.63818 |  |
| 563996.75 | 4191484.25 | 0.48700 | 564207.38 | 4191622.00 | 12.63402 |  |
| 564209.88 | 4191608.00 | 9.71392 | 564224.00 | 4191624.50 | 17.01254 | Berkeley City College Max |
| 564246.88 | 4191632.50 | 15.39784 | 564249.00 | 4191623.50 | 12.84499 |  |
| 564250.94 | 4191612.25 | 10.54765 | 564225.62 | 4191616.50 | 14.31199 |  |
| 564236.50 | 4191626.00 | 16.81191 | 564236.75 | 4191609.25 | 12.16590 |  |
| 564259.38 | 4191623.25 | 9.77541 |  |  |  |  |


| ISCST3 | *** Center St Garage | *** | 01/29/15 |
| :---: | :---: | :---: | :---: |
|  | *** Construction HRA | *** | 13:19:24 |
| **MODELOPTs: |  |  | PAGE 50 |

**MODELOPTs:
CONC
URBAN FLAT FLGPOL DFAULT
*** THE ANNUAL ( 3 YRS) AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: 2
INCLUDING SOURCE (S): L0000115, L0000116, L0000117, L0000118, L0000119, L0000120, L0000121, L0000122, L0000123, L0000124, L0000125, L0000126, L0000127, L0000128, L0000129, L0000130, L0000131, L0000132, L0000133, L0000134, L0000135, L0000136, L0000137, L0000138, L0000139, L0000140, L0000141, L0000142, L0000143, L0000144, . . .
*** DISCRETE CARTESIAN RECEPTOR POINTS ***
** CONC OF OTHER IN MICROGRAMS/M**3
X-COORD (M) Y-COORD (M)
X-COORD (M) Y-COORD (M)
CONC
564245.50 564263.62 564243.81 564263.81 564283.81 564303.81 564253.81 564273.81 564293.81 564243.81 564243.81 564263.81 564283.81 564273.63 564238.69 564172.25
564157.00
564172.25
564176.50 564176.50
564329.44 564329.44 564329.44 564319.44 564339.44 564329.44 564319.44 564339.44 564315.06 564315.06
564172.75 564172.75 564175.94 563892.50 563912.50 563882.50 563902.50
563922.50
563892.50
563912.50


CONC
564253.25
4191666.00
1.37585
$4191701.00 \quad 0.94049$
$564253.81-4191673.00 \quad 1.38538$
$564253.81-4191673.00 \quad 1.38538$
$\begin{array}{lll}564293.81 & 4191673.00 & 0.82301\end{array}$
$564243.81 \quad 4191683.00 \quad 1.65012$
$564263.81 \quad 4191683.00 \quad 1.21550$
$564283.81 \quad 4191683.00 \quad 0.93250$
$564301.94 \quad 4191683.25 \quad 0.75862$
$564253.81 \quad 4191693.00 \quad 1.42900$
$564273.81 \quad 4191693.00 \quad 1.42900$
$564273.81 \quad 4191693.00 \quad 1.06817$
$\begin{array}{lll}564293.81 & 4191693.00 & 0.83731 \\ 564293.81 & 4191703.00 & 0.84704\end{array}$
$\begin{array}{lll}564162.25 & 4191714.00 & 5.81865\end{array}$
$564182.25 \quad 4191716.50 \quad 5.21037$
$564162.25 \quad 4191724.00 \quad 6.77527$
$564182.25 \quad 4191724.00 \quad 5.65875$
$564319.44 \quad 4191713.75 \quad 0.65756$
$564319.44 \quad 4191723.75$. 656
$564319.44 \quad 4191723.75 \quad 0.66507$
$\begin{array}{lll}564339.44 & 4191723.75 & 0.55525\end{array}$
$\begin{array}{lll}564319.44 & 4191743.75 & 0.69657\end{array}$
$564339.44 \quad 4191743.75 \quad 0.57826$
$564329.44 \quad 4191753.75 \quad 0.65352$
$564312.69 \quad 4191749.50 \quad 0.76128$
$564172.75 \quad 4191830.50 \quad 10.19569$
$564174.06 \quad 4191808.25 \quad 10.98796$
$563882.50 \quad 4191825.50 \quad 1.98796$
$563902.50 \quad 4191825.50 \quad 8.30860$
$563922.50 \quad 4191825.50 \quad 11.93919$
$563892.50 \quad 4191835.50 \quad 4.24845$
$563912.50 \quad 4191835.50 \quad 8.18175$
$563882.50 \quad 4191845.50 \quad 2.34857$
$563902.50-4191845.50 \quad 5.12642$
7.70035

| 563882.50 | 4191855.50 | 2.18680 | 563892.50 | 4191855.50 | 3.13437 |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 563902.50 | 4191855.50 | 4.26599 | 563912.50 | 4191855.50 | 5.38695 |
| 563922.50 | 4191855.50 | 6.35764 | 56390.50 | 4191865.50 | 3.63967 |
| 563912.50 | 4191865.50 | 4.52836 | 563922.50 | 4191865.50 | 5.33870 |
| 563902.50 | 4191875.50 | 3.16639 | 563912.50 | 4191875.50 | 3.88071 |
| 563922.50 | 4191875.50 | 4.55699 | 564003.75 | 4191730.50 | 3.10213 |
| 563940.50 | 4191484.25 | 0.45768 | 563942.31 | 4191469.00 | 0.42970 |
| 563945.31 | 4191452.75 | 0.40416 | 563893.88 | 4191477.00 | 0.35633 |
| 563889.62 | 4191468.50 | 0.33772 | 563890.81 | 4191454.50 | 0.32149 |
| 563945.94 | 4191440.50 | 0.38381 | 563916.25 | 4191722.00 | 2.09018 |
| 563904.19 | 4191718.50 | 1.74422 | 563894.50 | 4191716.50 | 1.50388 |
| 563883.56 | 4191713.00 | 1.26333 | 564138.38 | 4191503.50 | 0.85650 Berkeley High School Max |
| 564143.25 | 4191467.25 | 0.72482 | 564146.88 | 4191414.00 | 0.57763 |
| 564093.00 | 4191495.75 | 0.72840 | 564040.38 | 4191490.25 | 0.64053 |
| 563996.75 | 4191484.25 | 0.56234 | 564207.38 | 4191622.00 | 1.99670 |
| 564209.88 | 4191608.00 | 1.76158 | 564224.00 | 4191624.50 | 1.79112 |

*** ISCST3 - VERSION 02035 *** *** Center St Garage
*** Construction HRA

| *** | $01 / 29 / 15$ |
| :--- | :--- |
| *** | $13: 19: 24$ |

**MODELOPTs:
CONC
URBAN FLAT FLGPOL DFAULT
*** THE SUMMARY OF MAXIMUM ANNUAL ( 3 YRS) RESULTS ***
** CONC OF OTHER IN MICROGRAMS/M**3
NETWORK
GROUP ID
AVERAGE CONC
RECEPTOR (XR, YR, ZELEV, ZFLAG) OF TYPE GRID-ID


| ISCST3 | ** Center St Garage | *** | 01/29/15 |
| :---: | :---: | :---: | :---: |
|  | *** Construction HRA | *** | 13:19:24 |
| **MODELOPTS: |  |  | PAGE 53 |
| CONC | FLGPOL DFAULT |  |  |

*** Message Summary : ISCST3 Model Execution ***
A Total of
0 Fatal Error Message(s)

A Total of
A Total of
0 Warning Message (s)

A Total of
52 Calm Hours Identified
******** FATAL ERROR MESSAGES ********
*** NONE ***
******** WARNING MESSAGES *******
*** NONE ***
$* * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * ~+~$ *** ISCST3 Finishes Successfully *** ***************************************)

| ISCST3 | ** Center St Garage | *** | 01/29/15 |
| :---: | :---: | :---: | :---: |
|  | *** Construction HRA | *** | 13:19:24 |
| **MODELOPTS: |  |  | PAGE 53 |
| CONC | FLGPOL DFAULT |  |  |

*** Message Summary : ISCST3 Model Execution ***
A Total of
0 Fatal Error Message(s)

A Total of
A Total of
0 Warning Message (s)

A Total of
52 Calm Hours Identified
******** FATAL ERROR MESSAGES ********
*** NONE ***
******** WARNING MESSAGES *******
*** NONE ***
$* * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * ~+~$ *** ISCST3 Finishes Successfully *** ***************************************)

## Appendix C. Risk Calculation Worksheets

## Appendix

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Table C1
Model Output Calculations
UNMITIGATED SCENARIO

| Source <br> (a) | ISCST3 Output Annual Average $\left(\mu \mathrm{g} / \mathrm{m}^{3}\right)$ <br> ( c ) | Pollutant <br> (b) | Emission Rates ${ }^{2}$ Average Daily (g/s) <br> (d) | Scalar ${ }^{3}$ <br> (e) | MER Concentration Annual Average $\left(\mu \mathrm{g} / \mathrm{m}^{3}\right)$ <br> (f) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| RECEPTOR: RESIDENCES |  |  |  |  |  |
| 2015 Onsite | 24.7 | $\begin{aligned} & \hline \mathrm{DPM} \\ & \mathrm{PM}_{2.5} \end{aligned}$ | $\begin{aligned} & \hline 3.10 \mathrm{E}-02 \\ & 3.60 \mathrm{E}-02 \end{aligned}$ | $\begin{aligned} & \hline 0.121 \\ & 0.121 \end{aligned}$ | $\begin{aligned} & 9.25 \mathrm{E}-02 \\ & 1.07 \mathrm{E}-01 \end{aligned}$ |
| 2015 Offsite | 1.82 | $\begin{aligned} & \hline \text { DPM } \\ & \mathrm{PM}_{2.5} \end{aligned}$ | $\begin{aligned} & 3.24 \mathrm{E}-05 \\ & 7.29 \mathrm{E}-05 \end{aligned}$ | $\begin{aligned} & \hline 0.121 \\ & 0.121 \end{aligned}$ | $\begin{aligned} & \hline 7.11 \mathrm{E}-06 \\ & 1.60 \mathrm{E}-05 \\ & \hline \end{aligned}$ |
| 2016 Onsite | 24.7 | $\begin{aligned} & \hline \text { DPM } \\ & \mathrm{PM}_{2.5} \end{aligned}$ | $\begin{aligned} & \hline 4.56 \mathrm{E}-02 \\ & 4.45 \mathrm{E}-02 \end{aligned}$ | $\begin{aligned} & \hline 0.912 \\ & 0.912 \end{aligned}$ | $\begin{aligned} & 1.03 \mathrm{E}+00 \\ & 1.00 \mathrm{E}+00 \end{aligned}$ |
| 2016 Offsite | 1.82 | $\begin{aligned} & \hline \text { DPM } \\ & \mathrm{PM}_{2.5} \end{aligned}$ | $\begin{aligned} & 1.30 \mathrm{E}-05 \\ & 6.88 \mathrm{E}-05 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 0.912 \\ & 0.912 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 2.17 \mathrm{E}-05 \\ & 1.14 \mathrm{E}-04 \\ & \hline \end{aligned}$ |
| RECEPTOR: BERKELEY CITY COLLEGE |  |  |  |  |  |
| 2015 Onsite | 17.0 | $\begin{aligned} & \hline \text { DPM } \\ & \mathrm{PM}_{2.5} \end{aligned}$ | $\begin{aligned} & \hline 3.10 \mathrm{E}-02 \\ & 3.60 \mathrm{E}-02 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.121 \\ & 0.121 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 6.36 \mathrm{E}-02 \\ & 7.39 \mathrm{E}-02 \\ & \hline \end{aligned}$ |
| 2015 Offsite | 1.79 | $\begin{aligned} & \hline \text { DPM } \\ & \mathrm{PM}_{2.5} \end{aligned}$ | $\begin{aligned} & 3.24 \mathrm{E}-05 \\ & 7.29 \mathrm{E}-05 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 0.121 \\ & 0.121 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 6.99 \mathrm{E}-06 \\ & 1.57 \mathrm{E}-05 \\ & \hline \end{aligned}$ |
| 2016 Onsite | 17.0 | $\begin{aligned} & \hline \text { DPM } \\ & \mathrm{PM}_{2.5} \end{aligned}$ | $\begin{aligned} & \hline 4.56 \mathrm{E}-02 \\ & 4.45 \mathrm{E}-02 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 0.912 \\ & 0.912 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 7.08 \mathrm{E}-01 \\ & 6.91 \mathrm{E}-01 \\ & \hline \end{aligned}$ |
| 2016 Offsite | 1.79 | $\begin{aligned} & \hline \text { DPM } \\ & \mathrm{PM}_{2.5} \end{aligned}$ | $\begin{aligned} & 1.30 \mathrm{E}-05 \\ & 6.88 \mathrm{E}-05 \\ & \hline \end{aligned}$ | $\begin{gathered} 0.912 \\ 0.912 \end{gathered}$ | $\begin{aligned} & 2.13 \mathrm{E}-05 \\ & 1.12 \mathrm{E}-04 \\ & \hline \end{aligned}$ |
| RECEPTOR: BERKELEY HIGH SCHOOL |  |  |  |  |  |
| 2015 Onsite | 1.05 | $\begin{aligned} & \hline \text { DPM } \\ & \mathrm{PM}_{2.5} \end{aligned}$ | $\begin{aligned} & \hline 3.10 \mathrm{E}-02 \\ & 3.60 \mathrm{E}-02 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 0.121 \\ & 0.121 \end{aligned}$ | $\begin{aligned} & \hline 3.92 \mathrm{E}-03 \\ & 4.56 \mathrm{E}-03 \\ & \hline \end{aligned}$ |
| 2015 Offsite | 0.86 | $\begin{aligned} & \hline \text { DPM } \\ & \mathrm{PM}_{2.5} \end{aligned}$ | $\begin{aligned} & 3.24 \mathrm{E}-05 \\ & 7.29 \mathrm{E}-05 \end{aligned}$ | $\begin{aligned} & \hline 0.121 \\ & 0.121 \end{aligned}$ | $\begin{aligned} & \hline 3.34 \mathrm{E}-06 \\ & 7.53 \mathrm{E}-06 \\ & \hline \end{aligned}$ |
| 2016 Onsite | 1.05 | $\begin{aligned} & \hline \text { DPM } \\ & \mathrm{PM}_{2.5} \end{aligned}$ | $\begin{aligned} & 4.56 \mathrm{E}-02 \\ & 4.45 \mathrm{E}-02 \end{aligned}$ | $\begin{aligned} & \hline 0.912 \\ & 0.912 \end{aligned}$ | $\begin{aligned} & \hline 4.37 \mathrm{E}-02 \\ & 4.26 \mathrm{E}-02 \end{aligned}$ |
| 2016 Offsite | 0.86 | $\begin{aligned} & \hline \text { DPM } \\ & \mathrm{PM}_{2.5} \end{aligned}$ | $\begin{aligned} & 1.30 \mathrm{E}-05 \\ & 6.88 \mathrm{E}-05 \end{aligned}$ | $\begin{aligned} & 0.912 \\ & 0.912 \\ & \hline \end{aligned}$ | $\begin{aligned} & 1.02 \mathrm{E}-05 \\ & 5.38 \mathrm{E}-05 \\ & \hline \end{aligned}$ |

${ }^{1}$ ISCST3 Output based on unit emission rates for sources ( $1 \mathrm{~g} / \mathrm{s}$ ).
${ }^{2}$ Emission Rates from Emission Rate Calculations (Appendix A - Input to ISCST3 Model).
${ }^{3}$ Scalar applied to adjust yearly ISCST3 concentrations to actual number of days construction emissions occur.
${ }^{4}$ Maximum exposed receptor (MER) pollutant concentration.

## Table C1

Model Output Calculations
MITIGATED SCENARIO - Level 3 Diesel Particulate Filters for Equipment 50 hp or greater

| Source <br> ( a ) | ISCST3 Output ${ }^{1}$ <br> Annual Average <br> $\left(\mu \mathrm{g} / \mathrm{m}^{3}\right)$ <br> (c) | Pollutant <br> (b) | Emission Rates ${ }^{2}$ <br> Average Daily <br> (g/s) <br> (d) | Scalar ${ }^{3}$ <br> (e) | MER Concentration ${ }^{4}$ <br> Annual Average <br> ( $\mu \mathrm{g} / \mathrm{m}^{3}$ ) <br> (f) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| RECEPTOR: RESIDENCES |  |  |  |  |  |
| 2015 Onsite | 24.7 | $\begin{aligned} & \hline \mathrm{DPM} \\ & \mathrm{PM}_{2.5} \end{aligned}$ | $\begin{aligned} & \hline 5.84 \mathrm{E}-03 \\ & 1.17 \mathrm{E}-02 \end{aligned}$ | $\begin{aligned} & \hline 0.121 \\ & 0.121 \end{aligned}$ | $\begin{aligned} & 1.74 \mathrm{E}-02 \\ & 3.48 \mathrm{E}-02 \end{aligned}$ |
| 2015 Offsite | 1.82 | $\begin{aligned} & \hline \text { DPM } \\ & \mathrm{PM}_{2.5} \end{aligned}$ | $\begin{aligned} & \hline 3.24 \mathrm{E}-05 \\ & 7.29 \mathrm{E}-05 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 0.121 \\ & 0.121 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 7.11 \mathrm{E}-06 \\ & 1.60 \mathrm{E}-05 \\ & \hline \end{aligned}$ |
| 2016 Onsite | 24.7 | $\begin{aligned} & \hline \text { DPM } \\ & \mathrm{PM}_{2.5} \end{aligned}$ | $\begin{aligned} & 1.07 \mathrm{E}-02 \\ & 1.05 \mathrm{E}-02 \end{aligned}$ | $\begin{aligned} & \hline 0.912 \\ & 0.912 \end{aligned}$ | $\begin{aligned} & \hline 2.40 \mathrm{E}-01 \\ & 2.37 \mathrm{E}-01 \\ & \hline \end{aligned}$ |
| 2016 Offsite | 1.82 | $\begin{aligned} & \text { DPM } \\ & \mathrm{PM}_{2.5} \end{aligned}$ | $\begin{aligned} & 1.30 \mathrm{E}-05 \\ & 6.88 \mathrm{E}-05 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 0.912 \\ & 0.912 \end{aligned}$ | $\begin{aligned} & 2.17 \mathrm{E}-05 \\ & 1.14 \mathrm{E}-04 \end{aligned}$ |
| RECEPTOR: BERKELEY CITY COLLEGE |  |  |  |  |  |
| 2015 Onsite | 17.0 | $\begin{aligned} & \hline \mathrm{DPM} \\ & \mathrm{PM}_{2.5} \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 5.84 \mathrm{E}-03 \\ & 1.17 \mathrm{E}-02 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 0.121 \\ & 0.121 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 1.20 \mathrm{E}-02 \\ & 2.39 \mathrm{E}-02 \\ & \hline \end{aligned}$ |
| 2015 Offsite | 1.79 | $\begin{aligned} & \hline \mathrm{DPM} \\ & \mathrm{PM}_{2.5} \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 3.24 \mathrm{E}-05 \\ & 7.29 \mathrm{E}-05 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 0.121 \\ & 0.121 \end{aligned}$ | $\begin{aligned} & \hline 6.99 \mathrm{E}-06 \\ & 1.57 \mathrm{E}-05 \end{aligned}$ |
| 2016 Onsite | 17.0 | $\begin{aligned} & \hline \text { DPM } \\ & \mathrm{PM}_{2.5} \end{aligned}$ | $\begin{aligned} & 1.07 \mathrm{E}-02 \\ & 1.05 \mathrm{E}-02 \\ & \hline \end{aligned}$ | $\begin{gathered} \hline 0.912 \\ 0.912 \end{gathered}$ | $\begin{aligned} & 1.65 \mathrm{E}-01 \\ & 1.63 \mathrm{E}-01 \\ & \hline \end{aligned}$ |
| 2016 Offsite | 1.79 | $\begin{aligned} & \hline \text { DPM } \\ & \mathrm{PM}_{2.5} \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 1.30 \mathrm{E}-05 \\ & 6.88 \mathrm{E}-05 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 0.912 \\ & 0.912 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 2.13 \mathrm{E}-05 \\ & 1.12 \mathrm{E}-04 \\ & \hline \end{aligned}$ |
| RECEPTOR: BERKELEY HIGH SCHOOL |  |  |  |  |  |
| 2015 Onsite | 1.05 | $\begin{aligned} & \hline \text { DPM } \\ & \mathrm{PM}_{2.5} \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 5.84 \mathrm{E}-03 \\ & 1.17 \mathrm{E}-02 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 0.121 \\ & 0.121 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 7.39 \mathrm{E}-04 \\ & 1.48 \mathrm{E}-03 \\ & \hline \end{aligned}$ |
| 2015 Offsite | 0.86 | $\begin{aligned} & \mathrm{DPM} \\ & \mathrm{PM}_{2.5} \end{aligned}$ | $\begin{aligned} & 3.24 \mathrm{E}-05 \\ & 7.29 \mathrm{E}-05 \end{aligned}$ | $\begin{aligned} & \hline 0.121 \\ & 0.121 \\ & \hline \end{aligned}$ | $\begin{aligned} & 3.34 \mathrm{E}-06 \\ & 7.53 \mathrm{E}-06 \end{aligned}$ |
| 2016 Onsite | 1.05 | $\begin{aligned} & \hline \mathrm{DPM} \\ & \mathrm{PM}_{2.5} \end{aligned}$ | $\begin{aligned} & 1.07 \mathrm{E}-02 \\ & 1.05 \mathrm{E}-02 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 0.912 \\ & 0.912 \\ & \hline \end{aligned}$ | $\begin{aligned} & 1.02 \mathrm{E}-02 \\ & 1.00 \mathrm{E}-02 \end{aligned}$ |
| 2016 Offsite | 0.86 | $\begin{aligned} & \text { DPM } \\ & \text { PM }_{2.5} \end{aligned}$ | $\begin{aligned} & 1.30 \mathrm{E}-05 \\ & 6.88 \mathrm{E}-05 \end{aligned}$ | $\begin{aligned} & \hline 0.912 \\ & 0.912 \end{aligned}$ | $\begin{aligned} & 1.02 \mathrm{E}-05 \\ & 5.38 \mathrm{E}-05 \end{aligned}$ |

${ }^{1}$ ISCST3 Output based on unit emission rates for sources ( $1 \mathrm{~g} / \mathrm{s}$ ).
${ }^{2}$ Emission Rates from Emission Rate Calculations (Appendix A - Input to ISCST3 Model).
${ }^{3}$ Scalar applied to adjust yearly ISCST3 concentrations to actual number of days construction emissions occur.
${ }^{4}$ Maximum exposed receptor (MER) pollutant concentration.

Construction Risk Assessment - Table C2
Adult Resident Exposure Scenario - 70 Years
Unmitigated Scenario

| Source | MER <br> Concentration <br> $\left(\mu \mathrm{g} / \mathrm{m}^{3}\right)$ <br> $(\mathrm{b})$ <br> 年 | Weight Fraction <br> ( c ) | Contaminant <br> (d) | Carcinogenic Risk |  |  | Noncarcinogenic Hazards/ Toxicological Endpoints ${ }^{*}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | $\begin{array}{\|c\|} \hline \text { CPF } \\ (\mathrm{mg} / \mathrm{kg} / \mathrm{day})^{-1} \\ \text { (e) } \end{array}$ | $\begin{gathered} \hline \text { DOSE ** } \\ (\mathrm{mg} / \mathrm{kg} / \mathrm{day}) \\ (\mathrm{f}) \\ \hline \end{gathered}$ | RISK <br> (g) | REL $\left(\mu \mathrm{g} / \mathrm{m}^{3}\right)$ (h) | ALI <br> (i) | BONE <br> (j) | CARDIO $(\mathrm{k})$ | DEV <br> (1) | ENDO $(\mathrm{m})$ | EYE <br> ( n ) | HEME <br> (o) | IMM <br> (p) | KID <br> (q) | NERV <br> (r) | REPRO <br> (s) | RESP <br> ( t$)$ | SKIN <br> (u) |
| 2015 On-Site Emissions | $9.25 \mathrm{E}-02$ | $1.00 \mathrm{E}+00$ | Diesel Particulate | $1.1 \mathrm{E}+00$ | $3.8 \mathrm{E}-07$ | 4.2E-07 | $5.0 \mathrm{E}+00$ |  |  |  |  |  |  |  |  |  |  |  | $1.8 \mathrm{E}-02$ |  |
| 2015 Truck Route | 7.11E-06 | $1.00 \mathrm{E}+00$ | Diesel Particulate | $1.1 \mathrm{E}+00$ | 2.9E-11 | 3.2E-11 | $5.0 \mathrm{E}+00$ |  |  |  |  |  |  |  |  |  |  |  | 1.4E-06 |  |
| 2016 On-Site Emissions | $1.03 \mathrm{E}+00$ | $1.00 \mathrm{E}+00$ | Diesel Particulate | $1.1 \mathrm{E}+00$ | 4.3E-06 | 4.7E-06 | $5.0 \mathrm{E}+00$ |  |  |  |  |  |  |  |  |  |  |  | $2.1 \mathrm{E}-01$ |  |
| 2016 Truck Route | $2.17 \mathrm{E}-05$ | $1.00 \mathrm{E}+00$ | Diesel Particulate | $1.1 \mathrm{E}+00$ | $9.0 \mathrm{E}-11$ | $9.9 \mathrm{E}-11$ | $5.0 \mathrm{E}+00$ |  |  |  |  |  |  |  |  |  |  |  | 4.3E-06 |  |
|  | BAAQMD Cancer Risk Adjustment Factor - 70-year Adult Scenaric |  |  |  |  | $\begin{gathered} 5.1 \mathrm{E}-06 \\ 1.7 \\ 8.6 \mathrm{E}-06 \end{gathered}$ |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.22 | 0.0 |

Key to Toxicological Endpoints

| ALI | Alonen |
| :--- | :--- |
| BONE | Alimentary |
| CARDIO | Cardiovascular |
| DEV | Developmental |
| ENDO | Endocrine |
| EYE | Eye |
| HEME | Hematologic |
| IMM | Immune |
| KID | Kidney |
| NERV | Nervous |
| REPRO | Reproductive |
| RESP | Respiratory |
| SKIN | Skin |

SKIN
Skin
** Exposure factors used to calculate dose
daily breathing rate (L/kg-day) - adult residen
inhalation absorption factor
$\begin{array}{ll}302 \\ & 1.0\end{array}$
$\begin{array}{ll}\text { exposure frequency (days/year) }- \text { residents } & 350 \\ \text { exposure duration (years) }-2015\end{array}$
exposure duration (years) - 2015
exposure duration (years) - 2016
averaging time (days) - 70 year duratio
fraction of time at home

2015 maximum annual PM2.5 concentration $\left(\mathrm{\mu g} / \mathrm{m}^{3}\right)$ 2016 maximum annual PM2.5 concentration $\left(\mu \mathrm{g} / \mathrm{m}^{3}\right)$

350
1.0
1.0

25,550
1.0
302
1.0
350
1.0
1.0
25,550
1.0

Construction Risk Assessment - Table C3
Adult Resident Exposure Scenario-70 Years

## With Mitigation (Level 3 Diesel Particulate Filters)

| Source | MER | Weight | Contaminant |  | arcinogenic R |  |  |  |  |  | Nonc | inogen | Hazar | Toxicolo | cal E | ints ${ }^{\text {a }}$ |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Concentration $\left(\mu \mathrm{g} / \mathrm{m}^{3}\right)$ (b) | Fraction <br> ( c ) |  | $\begin{array}{\|c\|} \hline \text { CPF } \\ (\mathrm{mg} / \mathrm{kg} / \mathrm{day})^{-1} \\ (\mathrm{e}) \end{array}$ | $\begin{gathered} \hline \text { DOSE }^{* *} \\ (\mathrm{mg} / \mathrm{kg} / \mathrm{day}) \\ (\mathrm{f}) \end{gathered}$ | RISK <br> (g) | REL $\left(\mu \mathrm{g} / \mathrm{m}^{3}\right)$ (h) | ALI <br> (i) | BONE <br> (j) | CARDIO $(\mathrm{k})$ | DEV <br> (1) | $\begin{gathered} \text { ENDO } \\ (\mathrm{m}) \end{gathered}$ | EYE <br> ( n ) | HEME <br> (o) | IMM <br> (p) | KID <br> (q) | NERV <br> (r) | REPRO <br> (s) | RESP <br> ( t$)$ | SKIN <br> (u) |
| 2015 On-Site Emissions | 1.74E-02 | $1.00 \mathrm{E}+00$ | Diesel Particulate | $1.1 \mathrm{E}+00$ | 7.2E-08 | $5.8 \mathrm{E}-08$ | $5.0 \mathrm{E}+00$ |  |  |  |  |  |  |  |  |  |  |  | 3.5E-03 |  |
| 2015 Truck Route | 7.11E-06 | $1.00 \mathrm{E}+00$ | Diesel Particulate | $1.1 \mathrm{E}+00$ | 2.9E-11 | $2.4 \mathrm{E}-11$ | $5.0 \mathrm{E}+00$ |  |  |  |  |  |  |  |  |  |  |  | 1.4E-06 |  |
| 2016 On-Site Emissions | $2.40 \mathrm{E}-01$ | $1.00 \mathrm{E}+00$ | Diesel Particulate | $1.1 \mathrm{E}+00$ | $9.7 \mathrm{E}-07$ | $7.8 \mathrm{E}-07$ | $5.0 \mathrm{E}+00$ |  |  |  |  |  |  |  |  |  |  |  | $4.8 \mathrm{E}-02$ |  |
| 2016 Truck Route | $2.17 \mathrm{E}-05$ | $1.00 \mathrm{E}+00$ | Diesel Particulate | $1.1 \mathrm{E}+00$ | 8.8E-11 | $7.1 \mathrm{E}-11$ | $5.0 \mathrm{E}+00$ |  |  |  |  |  |  |  |  |  |  |  | 4.3E-06 |  |
| TOTAL <br> BAAQMD Cancer Risk Adjustment Factor - 70-year Adult Scenaric |  |  |  |  |  | 8.4E-07 <br> 1.7 <br> $1.4 \mathrm{E}-06$ |  | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.05 | 0.00 |

Key to Toxicological Endpoints

| ALI | Alimentary <br> BONE |
| :--- | :--- |
| Conene | Cordiovascular |
| CARDIO | Cav |
| DEV | Developmental |
| ENDO | Endocrine |
| EYE | Eye |
| HEME | Hematologic |
| IMM | Immune |
| KID | Kidney |
| NERV | Nervous |
| REPRO | Reproductive |
| RESP | Respiratory |
| SKIN | Skin |

** Exposure factors used to calculate dose
daily breathing rate (L/kg-day) - adult residen 302
inhalation absorption factot $\quad 1.0$

| exposure frequency (days/year) | residents |
| :--- | :--- |
| exposure duration (years) -2015 | 350 |

$\begin{array}{ll}\text { exposure duration (years) - } 2015 & 1.0 \\ \text { exposure duration (years) }-2016 & 1.0\end{array}$
averaging time (days) - 70 year duration 25,550
fraction of time at home 0.73

2015 maximum annual PM2.5 concentration $\left(\mathrm{\mu g} / \mathrm{m}^{3}\right)$
0.03
0.24

Construction Risk Assessment - Table C4
Child Resident Exposure Scenario - 9 Years
Unmitigated Scenario

| Source | MER | Weight | Contaminant |  | arcinogenic R |  |  |  |  |  | No | nog | Hazard | Toxicolo | al | ints ${ }^{4}$ |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ( a) | Concentration $\left(\mu \mathrm{g} / \mathrm{m}^{3}\right)$ <br> (b) | Fraction <br> ( c ) |  | $\begin{array}{\|c\|} \hline \text { CPF } \\ (\mathrm{mg} / \mathrm{kg} / \mathrm{day})^{-1} \\ \text { (e) } \end{array}$ | $\begin{array}{\|c\|} \hline \mathrm{DOSE}^{* *} \\ (\mathrm{mg} / \mathrm{kg} / \mathrm{day}) \\ (\mathrm{f}) \end{array}$ | RISK <br> (g) | REL ( $\mu \mathrm{g} / \mathrm{m}^{3}$ ) (h) | ALI <br> (i) | BONE <br> (j) | CARDIO <br> (k) | DEV <br> (1) | ENDO <br> (m) | EYE <br> ( n ) | HEME <br> (o) | IMM <br> (p) | KID <br> (q) | NERV <br> (r) | REPRO <br> (s) | RESP <br> (t) | SKIN <br> (u) |
| 2015 On-Site Emissions | $9.25 \mathrm{E}-02$ | $1.00 \mathrm{E}+00$ | Diesel Particulate | $1.1 \mathrm{E}+00$ | 7.4E-07 | 8.1E-07 | $5.0 \mathrm{E}+00$ |  |  |  |  |  |  |  |  |  |  |  | $1.8 \mathrm{E}-02$ |  |
| 2015 Truck Route | 7.11E-06 | $1.00 \mathrm{E}+00$ | Diesel Particulate | $1.1 \mathrm{E}+00$ | $5.7 \mathrm{E}-11$ | 6.2E-11 | $5.0 \mathrm{E}+00$ |  |  |  |  |  |  |  |  |  |  |  | 1.4E-06 |  |
| 2016 On-Site Emissions | $1.03 \mathrm{E}+00$ | $1.00 \mathrm{E}+00$ | Diesel Particulate | $1.1 \mathrm{E}+00$ | 8.0E-06 | 8.8E-06 | $5.0 \mathrm{E}+00$ |  |  |  |  |  |  |  |  |  |  |  | $2.1 \mathrm{E}-01$ |  |
| 2016 Truck Route | $2.17 \mathrm{E}-05$ | $1.00 \mathrm{E}+00$ | Diesel Particulate | $1.1 \mathrm{E}+00$ | 1.7E-10 | $1.9 \mathrm{E}-10$ | $5.0 \mathrm{E}+00$ |  |  |  |  |  |  |  |  |  |  |  | 4.3E-06 |  |
| BAAQMD Cancer |  |  | TOTAL <br> Risk Adjustment Factor - 9-year Child Scenaric |  |  | $\begin{gathered} 9.6 \mathrm{E}-06 \\ 4.7 \\ 4.5 \mathrm{E}-05 \end{gathered}$ |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.22 | 0.0 |

Key to Toxicological Endpoints

| ALI | Alimentary |
| :--- | :--- |
| BONE | Bone |
| CARDIO | Cardiovascular |
| DEV | Developmental |
| ENDO | Endocrine |
| EYE | Eye |
| HEME | Hematologic |
| IMM | Immune |
| KID | Kidney |
| NERV | Nervous |
| REPRO | Reproductive |
| RESP | Respiratory |
| SKIN | Skin |

SKIN
Skin
** Exposure factors used to calculate dose
daily breathing rate (L/kg-day) - adult residen
inhalation absorption factor
exposure frequency (days/ y , 1.0
$\begin{array}{ll}\text { exposure frequency (days/year) }- \text { residents } & 350 \\ \text { exposure duration (years) }-2015 & 1.0\end{array}$
exposure duration (years) - 2015
exposure duration (years) - 2016
averaging time (days) - 70 year duration
fraction of time at home

2015 maximum annual PM2.5 concentration $\left(\mathrm{\mu g} / \mathrm{m}^{3}\right)$ 2016 maximum annual PM2.5 concentration $\left(\mu \mathrm{g} / \mathrm{m}^{3}\right)$

350
1.0
1.0
1.0

25,550
1.0
581
1.0
350
1.0
1.0
25,550
1.0

Construction Risk Assessment - Table C5
Child Resident Exposure Scenario - 9 Years

## With Mitigation (Level 3 Diesel Particulate Filters)

| Source | MER | Weight | Contaminant |  | arcinogenic Ri |  |  |  |  |  | Nonc | inogen | Hazar | Toxicolo | al En | ints ${ }^{\text {a }}$ |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Concentration $\left(\mu \mathrm{g} / \mathrm{m}^{3}\right)$ (b) | Fraction <br> ( c) |  | $\begin{array}{\|c\|} \hline \text { CPF } \\ (\mathrm{mg} / \mathrm{kg} / \mathrm{day})^{-1} \\ (\mathrm{e}) \\ \hline \end{array}$ | $\begin{gathered} \hline \text { DOSE }^{* *} \\ (\mathrm{mg} / \mathrm{kg} / \mathrm{day}) \\ (\mathrm{f}) \end{gathered}$ | RISK <br> (g) | REL $\left(\mu \mathrm{g} / \mathrm{m}^{3}\right)$ (h) | ALI <br> (i) | BONE <br> (j) | CARDIO $(\mathrm{k})$ | DEV <br> (1) | $\begin{gathered} \text { ENDO } \\ (\mathrm{m}) \end{gathered}$ | EYE <br> ( n ) | HEME <br> (o) | IMM <br> (p) | KID <br> (q) | NERV <br> (r) | REPRO <br> (s) | RESP <br> ( t$)$ | SKIN <br> (u) |
| 2015 On-Site Emissions | 1.74E-02 | $1.00 \mathrm{E}+00$ | Diesel Particulate | $1.1 \mathrm{E}+00$ | 1.4E-07 | 1.1E-07 | $5.0 \mathrm{E}+00$ |  |  |  |  |  |  |  |  |  |  |  | 3.5E-03 |  |
| 2015 Truck Route | 7.11E-06 | $1.00 \mathrm{E}+00$ | Diesel Particulate | $1.1 \mathrm{E}+00$ | $5.7 \mathrm{E}-11$ | 4.7E-11 | $5.0 \mathrm{E}+00$ |  |  |  |  |  |  |  |  |  |  |  | 1.4E-06 |  |
| 2016 On-Site Emissions | $2.40 \mathrm{E}-01$ | $1.00 \mathrm{E}+00$ | Diesel Particulate | $1.1 \mathrm{E}+00$ | 1.9E-06 | $1.5 \mathrm{E}-06$ | $5.0 \mathrm{E}+00$ |  |  |  |  |  |  |  |  |  |  |  | $4.8 \mathrm{E}-02$ |  |
| 2016 Truck Route | $2.17 \mathrm{E}-05$ | $1.00 \mathrm{E}+00$ | Diesel Particulate | $1.1 \mathrm{E}+00$ | 1.7E-10 | $1.4 \mathrm{E}-10$ | $5.0 \mathrm{E}+00$ |  |  |  |  |  |  |  |  |  |  |  | 4.3E-06 |  |
| BAAQMD Cancer |  |  |  | Risk Adjustment Factor - 9-year Child Scenaric Adjusted Cancer Risk |  | $\begin{aligned} & 1.7 \mathrm{E}-06 \\ & 4.7 \\ & 7.8 \mathrm{E}-06 \end{aligned}$ |  | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.05 | 0.00 |

Key to Toxicological Endpoints

| ALI | Alimentary |
| :--- | :--- |
| BONE | Bone |
| CARDIO | Cardiovascular |
| DEV | Developmental |
| ENDO | Endocrine |
| EYE | Eye |
| HEME | Hematologic |
| IMM | Immune |
| KID | Kidney |
| NERV | Nervous |
| REPRO | Reproductive |
| RESP | Respiratory |
| SKIN | Skin |

SKIN
Skin
** Exposure factors used to calculate dose
daily breathing rate (L/kg-day) - adult residen
inhalation absorption factor
exposure frequency (days/year) residents $\quad 1.0$
$\begin{array}{lr}\text { exposure frequency (days/year) - residents } & 350 \\ \text { exposure duration (years) }-2015 & 1.0\end{array}$
exposure duration (years) - 2015
exposure duration (years) - 2016
averaging time (days) - 70 year duration
fraction of time at home

2015 maximum annual PM2.5 concentration $\left(\mu \mathrm{g} / \mathrm{m}^{3}\right)$ 2016 maximum annual PM2.5 concentration $\left(\mu \mathrm{g} / \mathrm{m}^{3}\right)$

350
1.0
1.0
1.0 25,550
0.75
581
1.0
350
1.0
1.0
25,550
0.75

Construction Risk Assessment - Table C6
Berkeley City College Exposure Scenario
Unmitigated Scenario

| Source | MER | Weight | Contaminant |  | arcinogenic Ri |  |  |  |  |  | Nonc | inogen | Hazar | Toxicolo | cal E | ints ${ }^{\text {a }}$ |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Concentration $\left(\mu \mathrm{g} / \mathrm{m}^{3}\right)$ (b) | Fraction <br> ( c ) |  | $\begin{array}{\|c\|} \hline \text { CPF } \\ (\mathrm{mg} / \mathrm{kg} / \mathrm{day})^{-1} \\ (\mathrm{e}) \end{array}$ | $\begin{array}{\|c\|} \hline \begin{array}{c} \mathrm{DOSE}^{* *} \\ (\mathrm{mg} / \mathrm{kg} / \mathrm{day}) \\ (\mathrm{f}) \end{array} \\ \hline \end{array}$ | RISK <br> (g) | REL $\left(\mu \mathrm{g} / \mathrm{m}^{3}\right)$ (h) | ALI <br> (i) | BONE <br> (j) | CARDIO $(\mathrm{k})$ | DEV <br> (1) | $\begin{gathered} \text { ENDO } \\ (\mathrm{m}) \end{gathered}$ | EYE <br> ( n ) | HEME <br> (o) | IMM <br> (p) | KID <br> (q) | NERV <br> (r) | REPRO <br> (s) | RESP <br> ( t$)$ | SKIN <br> (u) |
| 2015 On-Site Emissions | $6.36 \mathrm{E}-02$ | $1.00 \mathrm{E}+00$ | Diesel Particulate | $1.1 \mathrm{E}+00$ | 1.8E-07 | 2.0E-07 | $5.0 \mathrm{E}+00$ |  |  |  |  |  |  |  |  |  |  |  | 1.3E-02 |  |
| 2015 Truck Route | $6.99 \mathrm{E}-06$ | $1.00 \mathrm{E}+00$ | Diesel Particulate | $1.1 \mathrm{E}+00$ | 2.0E-11 | 2.2E-11 | $5.0 \mathrm{E}+00$ |  |  |  |  |  |  |  |  |  |  |  | 1.45-06 |  |
| 2016 On-Site Emissions | 7.08E-01 | $1.00 \mathrm{E}+00$ | Diesel Particulate | $1.1 \mathrm{E}+00$ | $2.0 \mathrm{E}-06$ | 2.2E-06 | $5.0 \mathrm{E}+00$ |  |  |  |  |  |  |  |  |  |  |  | 1.4E-01 |  |
| 2016 Truck Route | $2.13 \mathrm{E}-05$ | $1.00 \mathrm{E}+00$ | Diesel Particulate | $1.1 \mathrm{E}+00$ | 6.0E-11 | $6.6 \mathrm{E}-11$ | $5.0 \mathrm{E}+00$ |  |  |  |  |  |  |  |  |  |  |  | 4.3E-06 |  |
| TOTAL <br> BAAQMD Cancer Risk Adjustment Factor - Adult Student/Staff Scenaric |  |  |  |  |  | $\begin{gathered} 2.4 \mathrm{E}-06 \\ 1.0 \\ 2.4 \mathrm{E}-06 \end{gathered}$ |  | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.15 | 0.00 |

Key to Toxicological Endpoints

| ALI | Alo |
| :--- | :--- |
| BONE | Alimentary |
| CARDIO | Cane |
| DEV | Cardiovascular |
| ENDO | Developmental |
| EYE | Endocrine |
| HEME | Eye |
| IMM | Hematologic |
| KID | Immune |
| NERV | Kidney |
| REPRO | Nervous |
| RESP | Reproductive |
| SKIN | Respiratory |
|  | Skin |

** Exposure factors used to calculate dose
daily breathing rate ( $\mathrm{L} / \mathrm{kg}$-day) - adult student/staff inhalation absorption factor
exposure frequency (days) $\quad 1.0$
$\begin{array}{lr}\text { exposure frequency (days/year) - adult student/staft } & 240 \\ \text { exposure duration (years) - } 2015\end{array}$
exposure duration (years) - 2015
240
1.0
1.0
averaging time (days) - 70 year duration
25,550

2015 maximum annual PM2.5 concentration $\left(\mu \mathrm{g} / \mathrm{m}^{3}\right)$ 2016 maximum annual PM2.5 concentration $\left(\mu \mathrm{g} / \mathrm{m}^{3}\right)$

Construction Risk Assessment - Table C7
Berkeley City College Exposure Scenario

## With Mitigation (Level 3 Diesel Particulate Filters)

| Source | MER | Weight | Contaminant |  | arcinogenic R |  |  |  |  |  | Nonc | inogen | Hazar | Toxicolo | cal E | ints ${ }^{\text {a }}$ |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Concentration $\left(\mu \mathrm{g} / \mathrm{m}^{3}\right)$ (b) | Fraction <br> ( c ) |  | $\begin{array}{\|c\|} \hline \text { CPF } \\ (\mathrm{mg} / \mathrm{kg} / \mathrm{day})^{-1} \\ (\mathrm{e}) \end{array}$ | $\begin{gathered} \hline \text { DOSE }^{* *} \\ (\mathrm{mg} / \mathrm{kg} / \mathrm{day}) \\ (\mathrm{f}) \end{gathered}$ | RISK <br> (g) | REL $\left(\mu \mathrm{g} / \mathrm{m}^{3}\right)$ (h) | ALI <br> (i) | BONE <br> (j) | CARDIO $(\mathrm{k})$ | DEV <br> (1) | $\begin{gathered} \text { ENDO } \\ (\mathrm{m}) \end{gathered}$ | EYE <br> ( n ) | HEME <br> (o) | IMM <br> (p) | KID <br> (q) | NERV <br> (r) | REPRO <br> (s) | RESP <br> ( t$)$ | SKIN <br> (u) |
| 2015 On-Site Emissions | 1.20E-02 | $1.00 \mathrm{E}+00$ | Diesel Particulate | $1.1 \mathrm{E}+00$ | 3.4E-08 | 3.7E-08 | $5.0 \mathrm{E}+00$ |  |  |  |  |  |  |  |  |  |  |  | $2.4 \mathrm{E}-03$ |  |
| 2015 Truck Route | $6.99 \mathrm{E}-06$ | $1.00 \mathrm{E}+00$ | Diesel Particulate | $1.1 \mathrm{E}+00$ | 2.0E-11 | 2.2E-11 | $5.0 \mathrm{E}+00$ |  |  |  |  |  |  |  |  |  |  |  | 1.45-06 |  |
| 2016 On-Site Emissions | 1.65E-01 | $1.00 \mathrm{E}+00$ | Diesel Particulate | $1.1 \mathrm{E}+00$ | 4.6E-07 | 5.1E-07 | $5.0 \mathrm{E}+00$ |  |  |  |  |  |  |  |  |  |  |  | 3.3E-02 |  |
| 2016 Truck Route | $2.13 \mathrm{E}-05$ | $1.00 \mathrm{E}+00$ | Diesel Particulate | $1.1 \mathrm{E}+00$ | 5.9E-11 | $6.5 \mathrm{E}-11$ | $5.0 \mathrm{E}+00$ |  |  |  |  |  |  |  |  |  |  |  | 4.3E-06 |  |
| TOTAL <br> BAAQMD Cancer Risk Adjustment Factor - Adult Student/Staff Scenaric |  |  |  |  |  | $\begin{gathered} 5.4 \mathrm{E}-07 \\ 1.0 \\ 5.4 \mathrm{E}-07 \end{gathered}$ |  | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.04 | 0.00 |

Key to Toxicological Endpoints

| ALI | Alimentary <br> BONE |
| :--- | :--- |
| CARDIO | Cone |
| Cardiovascular |  |
| DEV | Developmental |
| ENDO | Endocrine |
| EYE | Eye |
| HEME | Hematologic |
| IMM | Immune |
| KID | Kidney |
| NERV | Nervous |
| RERRO | Reproductive |
| RESP | Respiratory |
| SKIN | Skin |

** Exposure factors used to calculate dose
daily breathing rate ( $\mathrm{L} / \mathrm{kg}$-day) - adult student/staff inhalation absorption factor
exposure frequency (days/ (dear) $\quad 1.0$ $\begin{array}{lr}\text { exposure frequency (days/y year) - adult student/staft } & 240 \\ \text { exposure duration (years) - } 2015 & 1.0\end{array}$ exposure duration (years) - 2015
averaging time (days) - 70 year duration
25,550

2015 maximum annual PM2.5 concentration $\left(\mu \mathrm{g} / \mathrm{m}^{3}\right)$ 0.02 2016 maximum annual PM2.5 concentration ( $\mathrm{\mu} / \mathrm{m}^{3}$ )

Construction Risk Assessment - Table C8 Berkeley High School - Student Exposure Scenario

## Unmitigated Scenario

| Source | MER | Weight | Contaminant |  | arcinogenic R |  |  |  |  |  | Nonca | cinogenic | Hazard | Toxicolo | El | ints ${ }^{\text {4 }}$ |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Concentration $\left(\mu \mathrm{g} / \mathrm{m}^{3}\right)$ (b) | Fraction <br> ( c) |  | $\begin{gathered} \mathrm{CPF} \\ (\mathrm{mg} / \mathrm{kg} / \mathrm{day})^{-1} \\ (\mathrm{e}) \end{gathered}$ | $\begin{gathered} \hline \text { DOSE }^{* *} \\ (\mathrm{mg} / \mathrm{kg} / \mathrm{day}) \\ (\mathrm{f}) \end{gathered}$ | RISK <br> (g) | REL <br> $\left(\mu \mathrm{g} / \mathrm{m}^{3}\right)$ <br> (h) | ALI <br> (i) | BONE <br> (j) | CARDIO $(\mathrm{k})$ | DEV <br> (1) | $\begin{gathered} \hline \text { ENDO } \\ (\mathrm{m}) \end{gathered}$ | EYE <br> (n) | HEME <br> (o) | IMM <br> (p) | KID <br> (q) | NERV <br> (r) | REPRO <br> (s) | RESP <br> ( t$)$ | SKIN <br> (u) |
| 2015 On-Site Emissions | $3.92 \mathrm{E}-03$ | $1.00 \mathrm{E}+00$ | Diesel Particulate | $1.1 \mathrm{E}+00$ | $1.2 \mathrm{E}-08$ | 1.4E-08 | $5.0 \mathrm{E}+00$ |  |  |  |  |  |  |  |  |  |  |  | $7.8 \mathrm{E}-04$ |  |
| 2015 Truck Route | $3.34 \mathrm{E}-06$ | $1.00 \mathrm{E}+00$ | Diesel Particulate | $1.1 \mathrm{E}+00$ | 1.1E-11 | 1.2E-11 | $5.0 \mathrm{E}+00$ |  |  |  |  |  |  |  |  |  |  |  | $6.7 \mathrm{E}-07$ |  |
| 2016 On-Site Emissions | 4.37E-02 | $1.00 \mathrm{E}+00$ | Diesel Particulate | $1.1 \mathrm{E}+00$ | 1.4E-07 | 1.5E-07 | $5.0 \mathrm{E}+00$ |  |  |  |  |  |  |  |  |  |  |  | 8.7E-03 |  |
| 2016 Truck Route | $1.02 \mathrm{E}-05$ | $1.00 \mathrm{E}+00$ | Diesel Particulate | $1.1 \mathrm{E}+00$ | 3.2E-11 | 3.6E-11 | $5.0 \mathrm{E}+00$ |  |  |  |  |  |  |  |  |  |  |  | 2.0E-06 |  |
| TOTAL <br> BAAQMD Cancer Risk Adjustment Factor - High School Student Scenaric |  |  |  |  |  | $\begin{gathered} 1.7 \mathrm{E}-07 \\ 3.0 \\ 5.0 \mathrm{E}-07 \end{gathered}$ |  | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.01 | 0.00 |


| * Key to Toxicological | Endpoints |
| :--- | :--- |
| ALI | Alimentary |
| BONE | Bone |
| CARDIO | Cardiovascula |
| DEV | Developmental |
| ENDO | Endocrine |
| EYE | Eye |
| HEME | Hematologic |
| IMM | Immune |
| KID | Kidney |
| NERV | Nervous |
| REPRO | Reproductive |
| RESP | Respiratory |
| SKIN | Skin |

** Exposure factors used to calculate dose
body weight (kg) - high school student
daily breathing rate (M/day) - high school studen daily breathing rate (L/kg-day) - high school studen inhalation absorption factor
exposure frequency (days/year) - high school studen
exposure duration (years) - 2015
exposure duration (years) - 2016
averaging time (days) - 70 year duration $\quad 25,550$
2015 maximum annual PM2.5 concentration $\left(\mu \mathrm{g} / \mathrm{m}^{3}\right) \quad 0.005$
2016 maximum annual PM2.5 concentration $\left(\mu \mathrm{g} / \mathrm{m}^{3}\right) \quad 0.04$

Construction Risk Assessment - Table C9

## Berkeley High School - Student Exposure Scenario

With Mitigation (Level 3 Diesel Particulate Filters)

| Source | MER | Weight | Contaminant |  | arcinogenic R |  |  |  |  |  | Nonc | inogen | Hazar | Toxicolo | cal E | ints ${ }^{\text {a }}$ |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Concentration $\left(\mu \mathrm{g} / \mathrm{m}^{3}\right)$ (b) | Fraction <br> ( c ) |  | $\begin{array}{\|c\|} \hline \text { CPF } \\ (\mathrm{mg} / \mathrm{kg} / \mathrm{day})^{-1} \\ (\mathrm{e}) \\ \hline \end{array}$ | $\begin{gathered} \hline \text { DOSE }^{* *} \\ (\mathrm{mg} / \mathrm{kg} / \mathrm{day}) \\ (\mathrm{f}) \end{gathered}$ | RISK <br> (g) | REL $\left(\mu \mathrm{g} / \mathrm{m}^{3}\right)$ (h) | ALI <br> (i) | BONE <br> (j) | CARDIO $(\mathrm{k})$ | DEV <br> (1) | $\begin{gathered} \text { ENDO } \\ (\mathrm{m}) \end{gathered}$ | EYE <br> ( n ) | HEME <br> (o) | IMM <br> (p) | KID <br> (q) | NERV <br> (r) | REPRO <br> (s) | RESP <br> ( t$)$ | SKIN <br> (u) |
| 2015 On-Site Emissions | $7.39 \mathrm{E}-04$ | $1.00 \mathrm{E}+00$ | Diesel Particulate | $1.1 \mathrm{E}+00$ | 2.3E-09 | 2.6E-09 | $5.0 \mathrm{E}+00$ |  |  |  |  |  |  |  |  |  |  |  | 1.5E-04 |  |
| 2015 Truck Route | 3.34E-06 | $1.00 \mathrm{E}+00$ | Diesel Particulate | $1.1 \mathrm{E}+00$ | 1.1E-11 | 1.2E-11 | $5.0 \mathrm{E}+00$ |  |  |  |  |  |  |  |  |  |  |  | 6.7E-07 |  |
| 2016 On-Site Emissions | 1.02E-02 | $1.00 \mathrm{E}+00$ | Diesel Particulate | $1.1 \mathrm{E}+00$ | 3.2E-08 | 3.5E-08 | $5.0 \mathrm{E}+00$ |  |  |  |  |  |  |  |  |  |  |  | $2.0 \mathrm{E}-03$ |  |
| 2016 Truck Route | $1.02 \mathrm{E}-05$ | $1.00 \mathrm{E}+00$ | Diesel Particulate | $1.1 \mathrm{E}+00$ | 3.2E-11 | 3.5E-11 | $5.0 \mathrm{E}+00$ |  |  |  |  |  |  |  |  |  |  |  | $2.0 \mathrm{E}-06$ |  |
| TOTAL <br> BAAQMD Cancer Risk Adjustment Factor - High School Student Scenaric |  |  |  |  |  | 3.8E-08 <br> 3.0 <br> 1.1E-07 |  | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.002 | 0.00 |


| * Key to Toxicological | Endpoints |
| :--- | :--- |
| ALI | Alimentary |
| BONE | Bone |
| CARDIO | Cardiovascula |
| DEV | Developmental |
| ENDO | Endocrine |
| EYE | Eye |
| HEME | Hematologic |
| IMM | Immune |
| KID | Kidney |
| NERV | Nervous |
| REPRO | Reproductive |
| RESP | Respiratory |
| SKIN | Skin |

** Exposure factors used to calculate dose
body weight (kg) - high school student
daily breathing rate (M/day) - high school studen daily breathing rate (L/kg-day) - high school studen inhalation absorption factor
exposure frequency (days/year) - high school studen exposure duration (years) - 2015
exposure duration (years) - 2016
averaging time (days) - 70 year duration 1.0

25,550
2015 maximum annual PM2.5 concentration $\left(\mu \mathrm{g} / \mathrm{m}^{3}\right) \quad 0.001$ 2016 maximum annual PM2.5 concentration $\left(\mu \mathrm{g} / \mathrm{m}^{3}\right) \quad 0.01$

Construction Risk Assessment - Table C10 Berkeley High School - Staff Exposure Scenario

## Unmitigated Scenario



Key to Toxicological Endpoints

| * Key to | Toxicological |
| :--- | :--- |
| Endpoints |  |
| ALI | Alimentary |
| BONE | Bone |
| CARDIO | Cardiovascular |
| DEV | Developmental |
| ENDO | Endocrine |
| EYE | Eye |
| HEME | Hematologic |
| IMM | Immune |
| KID | Kidney |
| NERV | Nervous |
| REPRO | Reproductive |
| RESP | Respiratory |
| SKIN | Skin |

** Exposure factors used to calculate dose
daily breathing rate (L/kg-day) - adult staf
inhalation absorption factor
exposure frequency (days/year) - adult staft
exposure duration (years) - 2015
exposure duration (years) - 2016
302
1.0
1.0
240
exposure duration (years) - 2016
averaging time (days) - 70 year duratio
25,550

2015 maximum annual PM2.5 concentration $\left(\mu \mathrm{g} / \mathrm{m}^{3}\right)$
0.005

2016 maximum annual PM2.5 concentration $\left(\mu \mathrm{g} / \mathrm{m}^{3}\right)$
0.04

Construction Risk Assessment - Table C11
Berkeley High School - Staff Exposure Scenario

## With Mitigation (Level 3 Diesel Particulate Filters)

| Source(a) | MER <br> Concentration <br> $\left(\mu \mathrm{g} / \mathrm{m}^{3}\right)$ | Weight Fraction <br> ( c) | Contaminant <br> (d) | Carcinogenic Risk |  |  | Noncarcinogenic Hazards/ Toxicological Endpoints* |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | $\begin{array}{\|c\|} \hline \text { CPF } \\ (\mathrm{mg} / \mathrm{kg} / \mathrm{day})^{-1} \\ (\mathrm{e}) \\ \hline \end{array}$ | $\begin{gathered} \hline \text { DOSE }^{* *} \\ (\mathrm{mg} / \mathrm{kg} / \mathrm{day}) \\ (\mathrm{f}) \end{gathered}$ | RISK <br> (g) | REL $\left(\mu \mathrm{g} / \mathrm{m}^{3}\right)$ (h) | ALI <br> (i) | BONE <br> (j) | CARDIO $(\mathrm{k})$ | DEV <br> (1) | $\begin{gathered} \text { ENDO } \\ (\mathrm{m}) \end{gathered}$ | EYE <br> ( n ) | HEME <br> (o) | IMM <br> (p) | KID <br> (q) | NERV <br> (r) | REPRO <br> (s) | RESP <br> ( t$)$ | SKIN <br> (u) |
| 2015 On-Site Emissions | $7.39 \mathrm{E}-04$ | $1.00 \mathrm{E}+00$ | Diesel Particulate | $1.1 \mathrm{E}+00$ | 2.1E-09 | 2.3E-09 | $5.0 \mathrm{E}+00$ |  |  |  |  |  |  |  |  |  |  |  | 1.5E-04 |  |
| 2015 Truck Route | 3.34E-06 | $1.00 \mathrm{E}+00$ | Diesel Particulate | $1.1 \mathrm{E}+00$ | $9.5 \mathrm{E}-12$ | 1.0E-11 | $5.0 \mathrm{E}+00$ |  |  |  |  |  |  |  |  |  |  |  | 6.7E-07 |  |
| 2016 On-Site Emissions | 1.02E-02 | $1.00 \mathrm{E}+00$ | Diesel Particulate | $1.1 \mathrm{E}+00$ | 2.9E-08 | 3.2E-08 | $5.0 \mathrm{E}+00$ |  |  |  |  |  |  |  |  |  |  |  | $2.0 \mathrm{E}-03$ |  |
| 2016 Truck Route | $1.02 \mathrm{E}-05$ | $1.00 \mathrm{E}+00$ | Diesel Particulate | $1.1 \mathrm{E}+00$ | $2.9 \mathrm{E}-11$ | 3.2E-11 | $5.0 \mathrm{E}+00$ | 0.00 | 0.00 |  |  |  |  |  |  |  |  |  | $2.0 \mathrm{E}-06$ |  |
| TOTAL <br> BAAQMD Cancer Risk Adjustment Factor - Adult Staff Scenaric |  |  |  |  |  | $\begin{gathered} 3.4 \mathrm{E}-08 \\ 1.0 \\ 3.4 \mathrm{E}-08 \end{gathered}$ |  |  |  | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.002 | 0.00 |

Key to Toxicological Endpoints

| ALI | Alimentary <br> BONE |
| :--- | :--- |
| CARDIO | Cone |
| Cardiovascular |  |
| DEV | Developmental |
| ENDO | Endocrine |
| EYE | Eye |
| HEME | Hematologic |
| IMM | Immune |
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averaging time (days) - 70 year duration
postre duration (y) 70 year duratio
1.0
1.0

25,550

2015 maximum annual PM2.5 concentration $\left(\mu \mathrm{g} / \mathrm{m}^{3}\right)$
0.001

2016 maximum annual PM2.5 concentration $\left(\mu \mathrm{g} / \mathrm{m}^{3}\right)$

